

**RECENT STUDIES OF THE DEBUNCHER TO  
ACCUMULATOR  
TRANSFER EFFICIENCY**

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PBAR NOTE # 476

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**Abstract**

We present recent studies of the Debuncher to Accumulator (D/A) transfer efficiency. Based upon a model of the D/A beamline using the computer code *Turtle*, we find that at least 98 % of the Debuncher antiprotons should be able to be injected into the Accumulator. Moreover, we find that the D/A transfer efficiency is extremely sensitive to the beam position and angle through the large quad D6Q6. Finally, we outline some investigations which may be of some importance in future analyses of D/A transfer.

One of the nagging problems which has plagued the operation of the Antiproton Source has been the inability to consistently transfer more than 90% of the Debuncher antiprotons to the Accumulator. The D/A transfer efficiency has typically run between 60% and 85%.

At one time, there was some suspicion that the D/A transfer efficiency was not optimized with respect to the beam momentum in the Debuncher. Therefore, studies were undertaken during December, 1986 (See Log Book #10, pp.204-206) to examine this issue. The results are shown in Appendix A, where it is seen that the Debuncher momentum is close to being optimized. But even at the optimal  $\frac{\delta p}{p} \simeq 0.15\%$ , the D/A transfer efficiency is only  $\sim 75\%$ . It was further found that the settings of the skew quads, SQ 607 and SQ 100 had little effect on the D/A transfer efficiency.

It has been shown that the D/A transfer efficiency is very sensitive to the vertical beam size (See Log Book, 30Nov.87). For delayed extraction, a plot is shown in Fig. 1 of A:IBEAM/D:IBEM1 vs. settings of the Debuncher vertical scraper, D:TJ308. As is seen, there is a dramatic increase in the D/A transfer efficiency for small scraper settings.

## COMPUTER MODEL OF D/A LINE

The computer code *Turtle* was used to model the D/A beamline in order to identify aperture restrictions. A survey of the beamline is contained in Appendix B. During a recent shift, protons were stacked in the Accumulator at a rate of about 1500 microamps per hour. The magnet current settings for that shift were used in the *Turtle* model and are contained in Appendix C. Based upon the survey and magnet settings, the *Turtle* code shown in Appendix D was derived. Note that the code starts just upstream of D6Q10 and ends just downstream of A1Q4. Line 8 of the *Turtle* code specifies the initial phase space of the beam. Since after beam cooling in the Debuncher, the antiprotons during normal operation should have achieved  $(\epsilon_H, \epsilon_V) = (7\pi, 7\pi)$  mm-mrad, in the *Turtle* code we have specified  $\sigma_H, \sigma_{H'}, \sigma_V, \sigma_{V'}$  via

$$\epsilon_H = 7\pi \times 10^{-6} \text{m} = \frac{6\pi\sigma_H^2}{\beta_H}, \text{etc.,}$$

where  $\beta_H$  and  $\beta_V$  are the Design Report values of the beta functions just upstream of D6Q10. Also, from the Design Report we take  $\frac{\delta p}{p} = 0.2\%$  and momentum  $p = 8.91858$  Gev/c.

All the trims have the same angular deflection per Ampere =  $6.6846 \times 10^{-2}$  mrad/Amp.

In the Debuncher, the quadrupoles are on the supplies as designated below:

**Straight Section Quads (D:QSS)**

D10, 30, 50

plus 2,3,4,5, except D4Q5 and D2Q5, which are on the Dipole Bus

**Defocussing Quads (D:QD)**

D20, 40, 60

plus 6,8,10,12,14,16,18, except D6Q6, which is on the Dipole Bus

**Focussing Quads (D:QF)**

7,9,11,13,15,17,19

In the *Turtle* code, the small quad excitations are based upon the curves given in Pbar Note # 418. As an example, consider

$$\text{D6Q9 (SQC)} \quad l_m = 27.6''$$

$$\text{Current} = 244.5 \text{Amps}$$

First, use the Pbar Note #418 to enumerate

Amps	$\int Gdl$
------	------------

119.06	3.394
258.31	7.398
119.19	3.398
258.34	7.399
229.00	6.577
255.61	7.335
229.03	6.578
255.63	7.335

Then, for each of the data points use the linearity of the small quads to calculate  $\int Gdl$  for 244.5 Amps. Finally, average the eight calculated values for 244.5 Amps, obtaining 99.889 kG/m. All small quads in the Debuncher, D/A Line, and Accumulator were handled in this way.

Information about the large quad excitation is contained in Appendix E.

Information about TB1 and TB2 in the D/A Line is contained in Appendix F (See Dave Harding). They have a magnetic length of 60".

The small dipoles D6B7 (SDD-019) and D6B8 (SDD-018R) have a magnetic length of 65.37". Their strengths relative to SDD-001 is contained in Appendix G. Their currents should be such as to produce fields which would bend an 8.91858 Gev/c particle by  $\frac{1}{66}360^\circ = 5.455^\circ$ . For D6B7 this yields a field of  $B=17.0685$  kG; however, D6B8 has a shunt set to  $\Delta I = -12.76$  Amps (See p. C-7). Using

$$\frac{\Delta B/B}{\Delta I/I} = 0.71 \pm 0.01,$$

with  $I=1183.4$  Amps, one gets  $\Delta B = -0.130669$  kG, or a total magnetic field in D6B8 of  $B + \Delta B = 16.9378$  kG.

Septum excitation data is contained in Pbar Note #396 and in Appendix H below. The data are quite linear. The Debuncher extraction septum and the two Accumulator injection septa are handled identically. The second and third data points in Appendix H are used to predict a septum's excitation. Then the two computed excitations are averaged. Since the Appendix H data are for a nominal magnetic length of 80", we multiply our computed excitations by 80/84 since we take the septa magnetic lengths to be 84".

Information on the Debuncher extraction kicker is contained in Appendix I. We took  $\int B dl = 1.34$  kG-m and a magnetic length of 98.375", giving

B=0.536 kG.

The apertures for the small quadrupoles were taken from the design drawings for the magnets and star chambers. The small dipole beampipe was measured to be  $2\frac{9}{32}'' \times 6\frac{3}{8}''$  (OD). To get the ID for this and all other devices, a nominal wall thickness of 0.083" was used. For Tor 807, the ceramic gap was taken to be 2.245" as shown in Fig. 2. Finally, the SEM apertures were taken from design drawings.

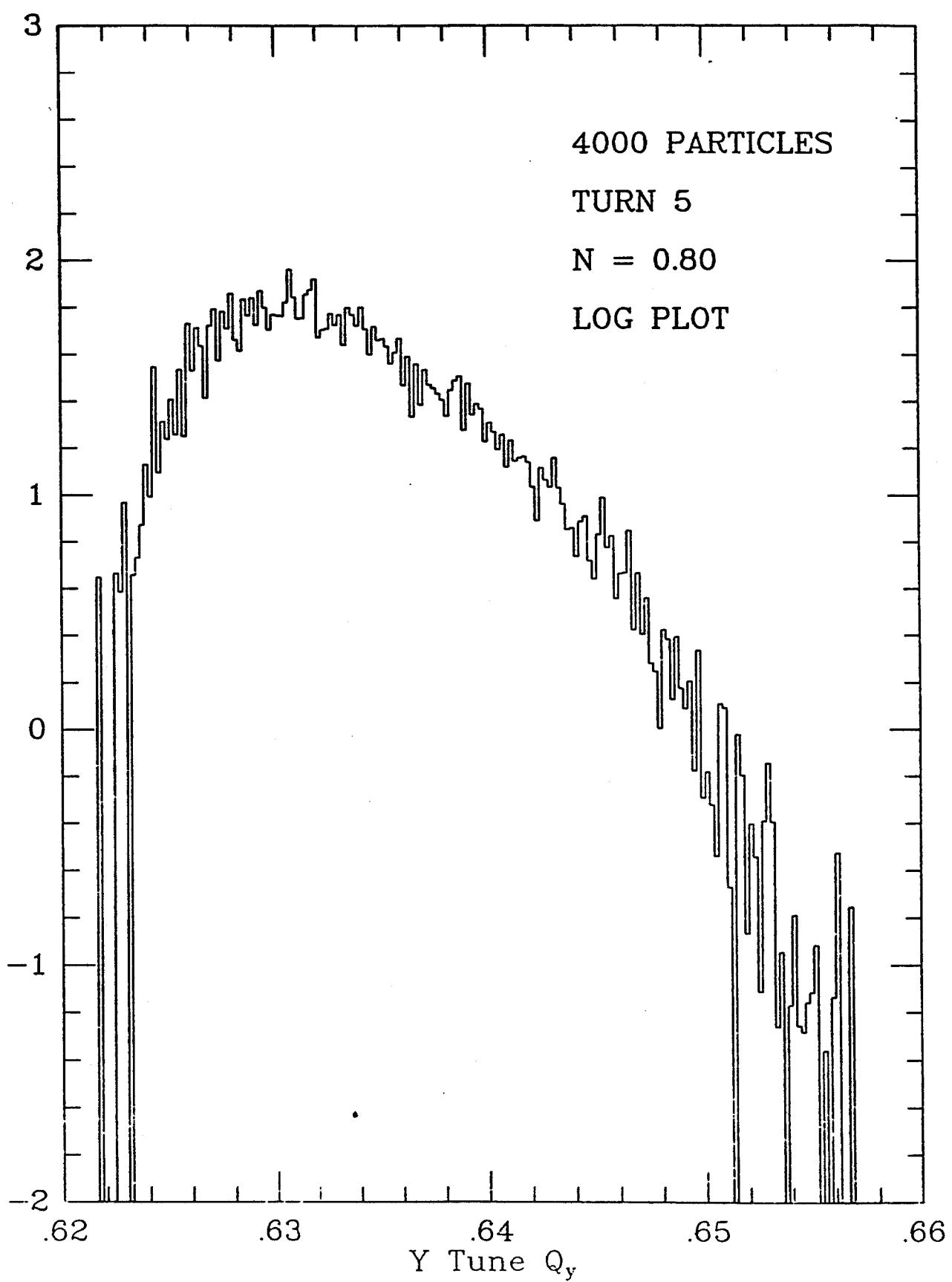


Figure 28

12-DEC-86

A-1

14:00 LINAC DOWN TO REPLACE P.A. EST. TIME  $\approx$  2 HRS.

Comments of scope traces of ~~beam~~ gap monitors (p201, 09:00)

All pictures taken with shutter open.  
~~beam~~ Sample of collimated Debuncher beam.

We see no dramatic fall-off in intensity either on the first few turns or on a longer time scale. Measuring the scope traces is hard, but under these conditions we rule out ~~20%~~ losses. Highly collimated beam is no better than uncollimated beam. This is quite puzzling since transmission (IBEAM/IBEF) is not 100%. See ~~not~~ previous pages

17:25 Mtingwa/Malamud.

(1) with 1.20 ma A: IBEAM reads 1.24 ma

with 1.20 ma D: IBEAM reads 1.24 ma.

These are scale factors since no beam offsets are much less. Therefore to first order A/D ratio is not affected.

(2) Set up to measure ratios as a function of P<sub>Debuncher</sub>

17:40 Booster off = Quad in ~~Booster~~, M: QFB4

17:45 Beam back

We have measured three ratios as a function of momentum,

TDR 807, A:IBEAM, 2<sup>nd</sup> turn on gap monitor.

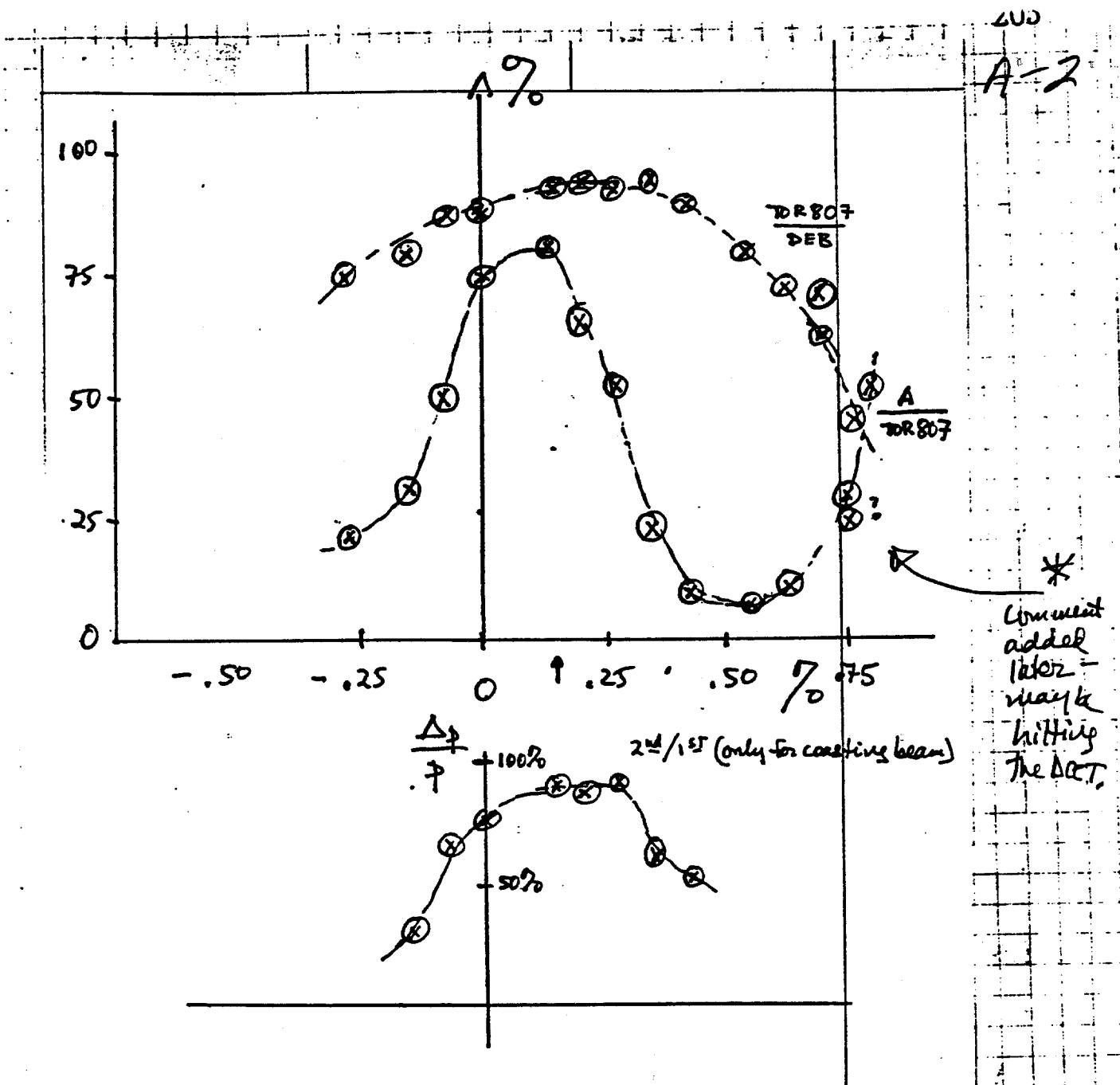
D:IBEAM , TDR 807

1<sup>st</sup> turn

Raw data, calculations, and machine settings are in hard copy log.

	<u>D/A acceptance</u>	<u>Accept</u>	<u>D/A, st</u>
peak	$\pm 0.25\%$	$\pm 0.10\%$	$\pm 0.20\%$
FWHM	1.0%	0.4%	

D/A efficiency vs Deb momentum



### Conclusions and questions

- Curves do not peak at same momentum.
- D/A looks reasonable. Maximum is  $\sim 95\%$ . Why not 100%? Is this a calibration error? Curve might have a plateau.
- Accumulator's we don't understand rise for  $p > .50\%$ . D/A transmission drops off smoothly. Coasting beam and then second turn vertices, yet Accumulator DCCT shows significant circulating current. [see \*]

2130 Based on momentum scan we will set at

$$\nu_{\text{Bob}} = 590023 \text{ Hz} \rightarrow \Delta p = +15\%$$

(3) Next we will play with skew Quads.

The nominal settings are supposed to be:

	SQ 607	SQ 100
no coupling on core	10	130
no coupling on injection orbit	30	100

we have done a "2-dimensional scan"

0 to 40      100 to 170

- The gap monitor picture looks about the same for all values,
- The efficiency A<sub>2</sub>TB84M/D<sub>B</sub>TOR807 remains at  $(80 \pm 2)\%$  for all values.

Data is in hand copy tag but probably not useful

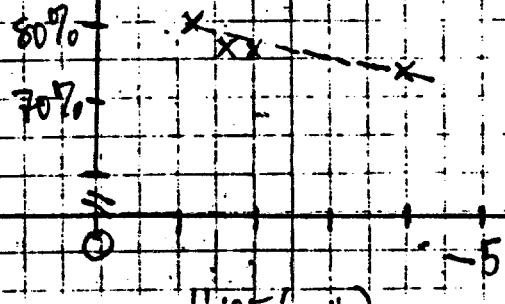
(4) Restored SQ value to 10, 130.

Vary bump

A108

A

TOR807



## APPENDIX B

'15

B-

MIKE GORMLEY

15-OCT-87

D→A LINE ("SURVEY")

Physical lengths

(INCHES)

<u>DEVICE</u>	<u>LENGTH</u>	<u>TRANSVERSE DIMENSIONS</u>
DRIFT	13.0	CIRCULAR OD = 5.505"
H-TRIM	18.375	"
DRIFT	17.0	(SEE FIGURE - 1)
D:ESEP	84.0	CIRCULAR OD = 2.62"
DRIFT	14.5 14.75	(SEE FIGURE - 2)
D6Q6	29.875	
DRIFT	13.0	CIRCULAR OD = 2.61"
DRIFT	188.75	"
Q1	59.125	STAR CHAMBER
DRIFT	31.75	CIRCULAR OD = 5.51"
TRIM	18.375	"
DRIFT	47.0	"
Q2	31.0 31.25	STAR CHAMBER
DRIFT	17.5	CIRCULAR OD = 5.51
SEM802	15.75	
DRIFT	99.5	CIRCULAR OD = 5.51
TRIM	18.5	"
DRIFT	36.5	"
Q3	31.25	STAR CHAMBER
DRIFT	26.	CIRCULAR OD = 5.51
Q4	25.75 25.68	STAR CHAMBER
DRIFT	124.5	CIRCULAR OD = 5.51
Q5	31.25	STAR CHAMBER
DRIFT	85.5	CIRCULAR OD = 5.50
Q6	31.25	STAR CHAMBER
DRIFT	13.0	CIRCULAR OD = 5.50
TRIM	18.5	"
DRIFT	188.5	OD = 4.06
IC	13.0	5.5
DRIFT	13.875	CIRCULAR OD = 5.52
SEM804	13.0	5.5
DRIFT	16.0	CIRCULAR OD = 5.52
BEND	60.0	RECTANGULAR HEIGHT = 2.30" WIDTH = 5.43"
DRIFT	12.75	CIRCULAR OD = 6.00
BEND	60.0	RECTANGULAR HEIGHT = 2.30" WIDTH = 5.43"
DRIFT	20.25	CIRCULAR OD = 5.45
Q7	16.75	STAR CHAMBER
	16.65	

#4

D→A LINE SURVEY (CONT.)

<u>DEVICE</u>	(INCH) <u>LENGTH</u>	<u>TRANSVERSE DIMENSIONS</u>	
Q7			
DRIFT	79.875	CIRCULAR	OD = 2.51
SEM 807	13.0		
DRIFT	48.75	CIRCULAR	OD = 2.60
A:ISEP1	84.		
DRIFT	3.75	CIRCULAR	OD = 2.62
A:ISEP2	84.		
DRIFT	13.75		
A: A1Q4	16.75	(SEE FIGURE-3)	

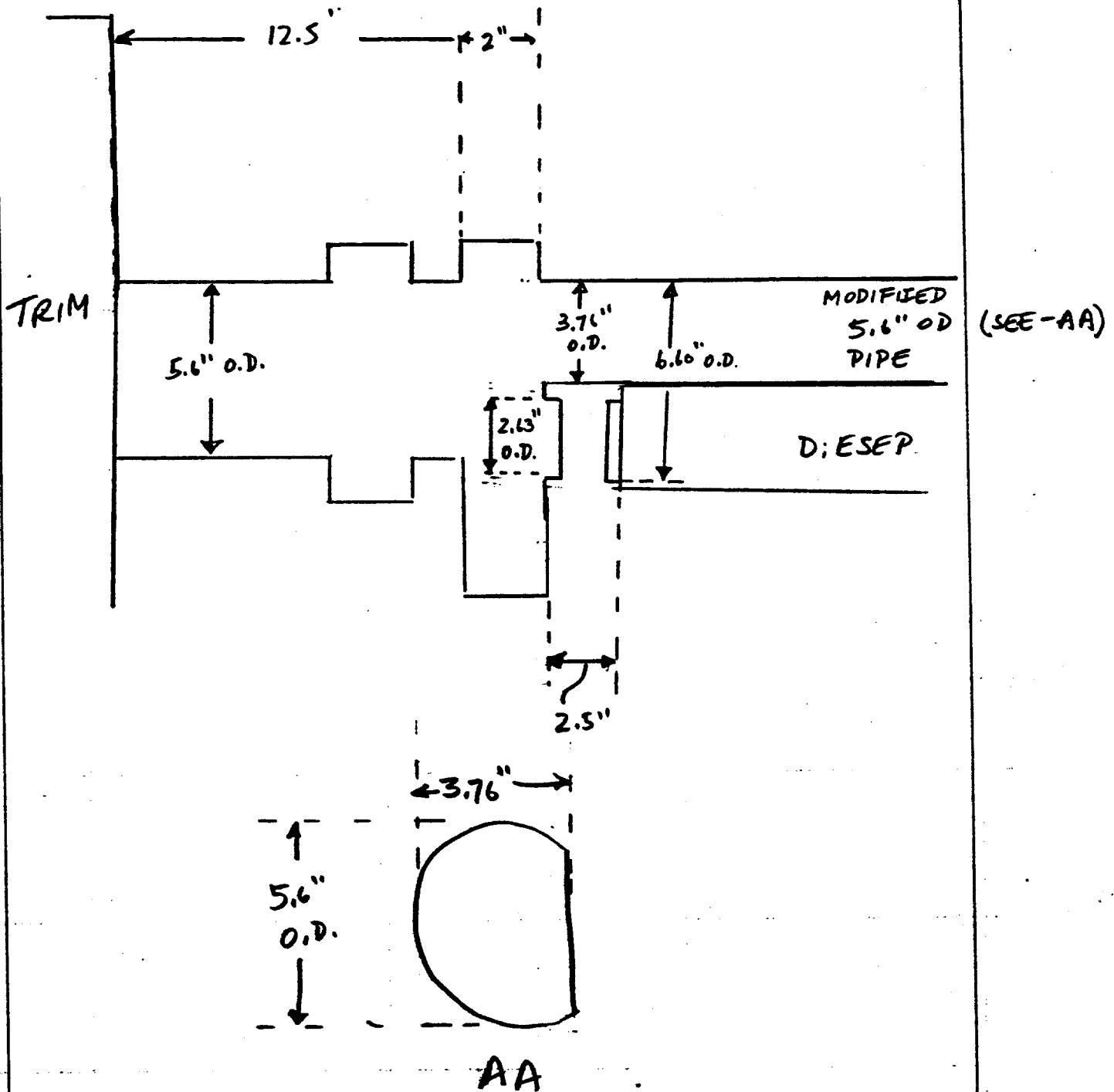
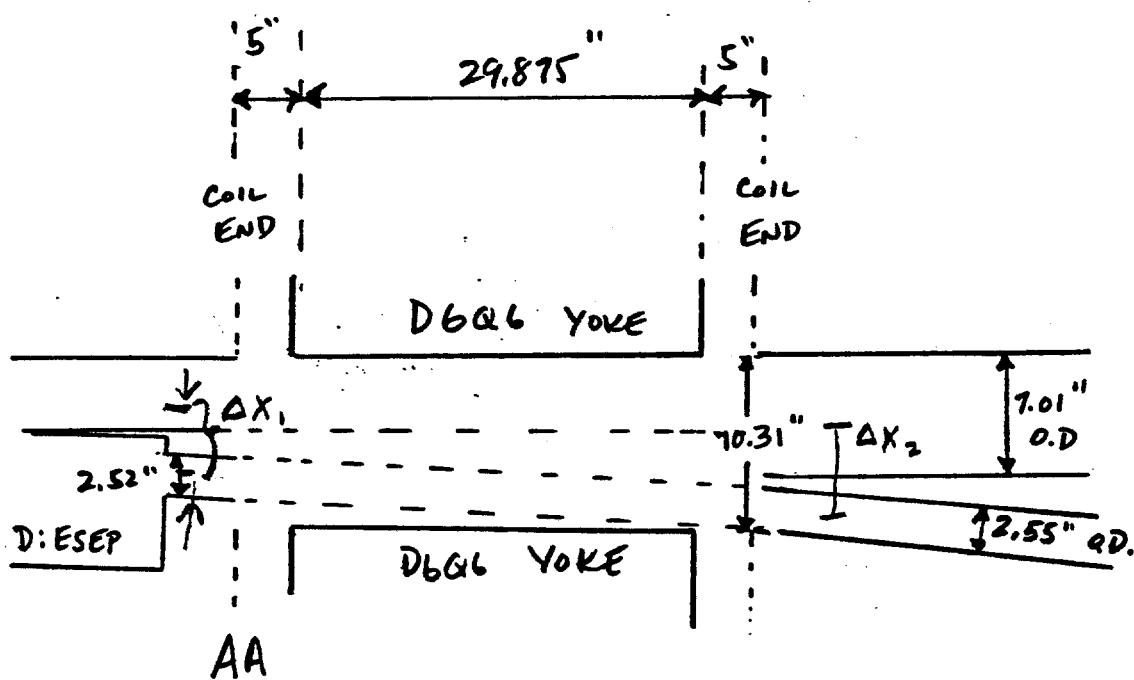
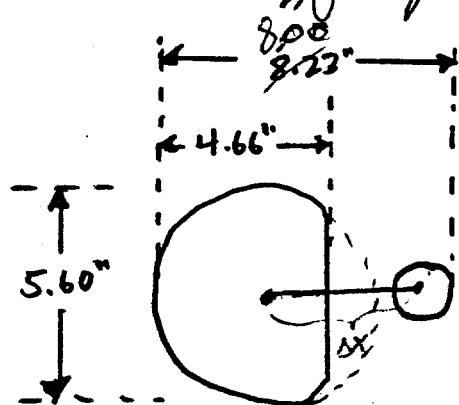


FIGURE - 1  
DEBUNCHER EXTRACTION LAYOUT  
BIRDS-EYE-VIEW



At split of septum



$$\Delta x_1 = 8.00 - \frac{5.60}{2} - \frac{2.52}{2} = 3.94$$

$$\Delta x_2 = 6.25$$

AA  
(LOOKING INTO D6Q6)

FIGURE - 2  
D6Q6 LAYOUT  
BIRDS-EYE-VIEW

2/5 B-5

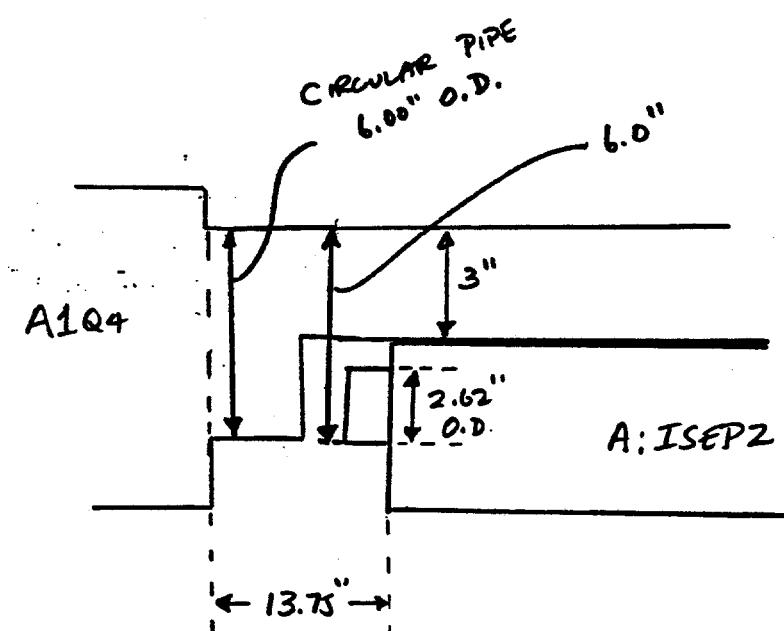


FIGURE - 3  
ACCUMULATOR INJECTION LAYOUT  
BIRDS-EYE-VIEW

APPENDIX C

stacking at  $\geq 1500 \text{ mAh}/\text{hr}$

MON 04-JAN-98 11:43

C-2

		WED 16-DEC-87 14:42			
D1 CHANNEL	Display File <692>	06-Dec-87 2310 Sun	.....	COPIES	RETURN
linac	booster	mainring switchyd levatron P-BAR_SR retrig	.....	.....	.....
proton	target	injectin d to a	extractn bstr lin rest	1	PAUX_DEV mainline
DEBUNCH	debunch	accumu	API0 API0/30	AP30/50	AP0/12
BUS	shunt	trin	inject	temp	studies
		A/D	A/D	A/D	A/D
-D:13	1183	1183.4	AMP	-D:18TEST	20 -2
-D:QF	244.1	244.5	AMP		
-D:QD	238.9	238.5	AMP		
-DIQSS	285.9	286.2	AMP		
-D:QT205	351.8	350.2	AMP		
-D:QT405	351.8	350	AMP		
-D:QT606	348.8	347.3	AMP		
-D:SEXFI	162.8	161	AMP		
-D:SEXFY	162.8	161.3	AMP		
-D:SEXDI	217.5	216.4	AMP		
-D:SEXDY	217.5	216.1	AMP		

$$\text{D}\sigma \text{ current} = 1183.4 + 347.3 = 1530.7$$

C-3

WED 16-DEC-87 14:36

D1 Display File <692> 06-Dec-87 2310 Sun

• COPIES • RETURN

CHANNEL ..... . . . . .

linac booster main ring switchyd tevatron P-BAR-SR rerrig sequencr system\_9

proton target injectin D TD A extractn bstr lin rest 1 pux-dev mainring  
debunch accumu ap10 ap10/30 ap30/50 ap50 ap0/r2  
times lossmon pu sup ..... . . . . .

D/A A/D D/A A/D

-DIQ801	241.9	240.9	AMP
-DIQ804	181	180.7	AMP
-DIQ807	43.1	43.02	AMP
-DIH807A	624	620	AMP
TB1	625.5	621.3	AMP
TB2	-DIH807B	-19.96	AMPS
	-DIQ8902	-15	AMPS
	-DIQ8903	-12.98	AMPS
	-DIQ8904	-2.34	AMPS
	-DIQ8906	2.3	
-DIVT801	4	3.974	AMP
-DIHT904	-5	-613	AMP
-DIVT806	-3	-2.976	AMP

(SQE) Q1 = D1Q801 = 240.9 A

(SQD) Q2 = D1Q801 - 19.96 = 220.94 A

(SQD) Q3 = 240.9 - 15 = 225.9 A

(SQC) Q4 = 180.7 - 12.98 = 167.72 A

(SQD) Q5 = 180.7 A

(SQD) Q6 = 180.7 - 2.34 = 178.36 A

..... . . . . .

C-4

MON 04-JAN-88 11:47

DI CHANNEL	DISPLAY FILE <698>	06-Dec-87 2310 Sun	COPIES+ RETURN
linac booster mainring switched tevatron P-BAR_SR reprise	sequencer system_9		HUPulse PAIR
proton target injection D TO A extractin bbar lin rest	1	pxux-dev rest 2	
debunch debunch accubar ip10 ip10/30 ip30/30	1	ip50 ap0/92	
TIMES lessonon pu sup	.....	.....	studles
.....			
D/A	A/D	D/A	A/D
-D1SMASS .0000874	.0000274	.000274	.000274
-D1SMAGC 0	0	SECS	SECS
-D1EXTRAT .497	.497	SECS	SECS
-D1ESEPM 20	20	USEC	SECS
-D1ESEPC 0	0	SECS	SECS
-AI1SEP10 54	54	USEC	SECS
-AI1SEP20 54	54	USEC	SECS
-AI1SEP1C 0	0	SECS	SECS
-AI1SEP2C 0	0	SECS	SECS
-AIISCRS 0	0	SECS	SECS

C-5

FRI 18-DEC-87 10:59

display file <692>	06-Doc-87	2310 Sun	•COPIES•	ERINNEX
PRINTS	.....	.....	.....	.....
line 5 booster mainring switchyd tevatron P-BAR-SR refit	.....	.....	.....	.....
program	injection d to a	extractn bstr lin rest	! PUX-dev monitor	.....
segment	asynch accumu	api0 ap30 ap30/c	.....	.....
404	shunt trim inject	EXTRACT bpa diag temp	.....	studies
D/A	A/D	D/A	A/D	A/D
-DISCEP	695	= 405.3	VOLT	
-DIEKIP	62	- 123	KV	
-DIEKIXM1	273.192	USEC		
-DIEKIXM2	273.278	USEC		
-DIEKIXM3	273.213	USEC		
-DIEKIXM4	276.306	USEC		
-DISCEPDM	20	20	USEC	

C-6

FRI 19-DEC-87 10:39

	D/A	A/D	D/A	A/D
-D1EIXIKM1	273.192		-D1H807A	624
-A1IKIKM1	272.368		-D1H807B	625.5
-Y1ESCPCH	20	20	-DIVT801	4
-A1ISCPD1	54	54	-DIVT806	-3
-S1ISCPG0	54	54	USEC	
-D1EKIK	62	-003	KV	-D1EKIKM1
-A1IKIK	63	-093	KV	-D1EKIKM2
-A1IXIKP	63	-043	KV	-D1EKIKM3
-A1ISCPV4	661.1	# 448.5	VOLT	-D1EKIKM4
-A1ISCPZ4	660.2	# 429.7	VOLT	
-D1ESCPY	695	# 403.5	VOLT	-A1IKIKM1
-A1ISCP11		-21136	AMPS	272.368
-A1ISCP21		-19049	AMPS	-A1IKIKM2
-A1ISCP31		-23086	AMPS	272.42
-A1ISCP41	0	0	SECS	-A1IKIKM3
-A1ISCP51	0	0	SECS	76.7
				SECS

\*COPIES\* \*PRINTED\*

Supstate page

Sequence system

PAUX\_GEN running

AP50 AP50/42

Motors startup

target injection to 2 extract bin rest 1

Launch deboost ACCUMU API0 API0/30 API0/50

shunt trim INJECT extract APA dampers diag

booster mainring switchyd levatron P-BAR\_SR refrig

display File# (692)

06-Dec-87 2310 Sun

۱۰

FRI 29-JAN-88 14:54

-A11B	ACCUMLATOR DIPPLE BU	1170.245	1170.127	A&P	...
-D1QS605	D605	50A QUAD MAG S	51	W-50.98	AMPS
-D1QS604	D604	20A QUAD MAG S	2.777	W-2.871	AMPS
-D1QS603	D603	50A QUAD MAG S	26.21	W-26.23	AMPS
-D1QS602	D602	50A QUAD MAG S	30.62	W-30.6	AMPS
-D1QS101	D101	20A QUAD MAG S	12.66	W-12.67	AMPS
-D1QS102	D102	50A QUAD MAG S	30.62	W-30.38	AMPS
-D1QS103	D103	50A QUAD MAG S	26.21	W-26.2	AMPS
-D1QS104	D104	20A QUAD MAG S	2.777	W-2.781	AMPS
-D1QS105	D105	50A QUAD MAG S	51	W-50.95	AMPS
-D1QS106	D106	20A QUAD MAG S	4.2	W-4.191	AMPS
-D1QS608	D608	25A DIPPLE SHUNT	12.73	W-12.76	AMP
-D1QS106	D106	ESTER TO IEE KICKER T	-19882		SCRS

C-8

DI CHANNEL	Display File <692>	06-Dec-87 2310 Sun	COPIES RETURN
LINAC BOOSTER	switching between P-BAR-SR retrig	.....	update p190
PROTON DEBUNCH BUS	target injectin d to a extractn bair lin rest 1	peux-dev rest 2	sequencer system_9
shunt trim	ACCUMU accumu sp10 sp10/30 sp30/30	sp30	sp30/s2
	inject extract spn dampers diag	motors	situations
	D/A	A/D	A/D
-AI:ID	1170	1170.382	AMP
-AI:LQ	1271	1270.834	AMP
-AI:QDF	239.3	239.307	AMP
-AI:QT	259.7	259.696	AMP
-AI:QSF1	3.477	-3.59	AMP
-AI:QSD	1.405	-1.4	AMP
-AI:SEX2	39.94	39.47	AMP
-AI:SEX7	43.4	41.92	AMP
-AI:SEX9	262.4	266.9	AMP
-AI:SEX10	397.2	395.2	AMP
-AI:SEX12	408.1	405.9	AMP
-AI:SQ100	44.9	45.22	AMP
-AI:SQ607	.159	.05	AMP
-AI:DCT10	46.7	46.37	AMP
-AI:DCT12	34.6	34.4	AMP
ANALYSIS		GAUS	

$$(SQA) \quad A/QY = A; QDF - 3.59 = 239.307 - 3.59 \\ = 235.717$$

'DEBUNCHER TO ACCUMULATOR TRANSFER LINE'  
(STARTING JUST US OF D6Q10 AND ENDING JUST DS OF A1Q4)  
(FEBRUARY 5, 1988)

D-1

10000

15. 1.0 'MM' .10 ;

15. 8.0 'IN' .02540 ;

13. 10. ;

1. 2.527 0.462 4.115 0.284 9332.0 0.1 8.91858;

(LINE BEGINS JUST UPSTREAM OF D6Q10.)

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16.0 100. 70.409 ;

16.0 101. 41.707 ;

5.0 'DG10' 27.6 -9.7438 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16.0 100. 67.8053 ;

16.0 101. 100. ;

5.0 'DRIF' 20.1275 0.0 100. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 48.6918 ;

5.0 'DRIF' 4.75 0.0 100. ;

(EKIK APERTURE)

16.0 4.0 38.100 ;

16.0 5.0 22.225 ;

2.0 0.129 ;

4.0 'EKIK' 98.375 0.536 0.0 ;

2.0 0.129 ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 48.6029 ;

5.0 'DRIF' 4.75 0.0 100. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 68.1228 ;

5.0 'DRIF' 18.8975 0.0 100. ;

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16.0 100. 70.409 ;

16.0 101. 41.707 ;

5.0 'D6Q9' 27.6 9.9889 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16.0 100. 67.7418 ;

16.0 101. 100. ;

5.0 'DRIF' 40.76 0. 100. ;

(D6B8 APERTURE)

16.0 4.0 78.8543 ;

16.0 5.0 26.8637 ;

2.0 2.7088 ;

4.0 'D6B8' 65.37 16.9378 0. ;

2.0 2.7088 ;

5.0 'DRIF' 40.76 0. 100.. ;

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16.0 100. 70.409 ;

16.0 101. 41.707 ;

5.0 'D6B8' 27.6 -9.7438 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16.0 100. 67.7418 ;

16.0 101. 100. ;

5.0 'DRIF' 40.76 0. 100. ;

2.0 2.7297 ;

4.0 'D6B7' 65.37 17.0685 0. ;

2.0 2.7297 ;

5.0 'DRIF' 14.76 0. 100. ;

(CIRCULAR SEM APERTURE)

16.0 100. 69.850 ;

5.0 'DRIF' 7.875 0. 100. ;

(OBTAIN SEM 607 PROFILES)

50. 1.0 -10. 10. 1.0 ;

50. 3.0 -10. 10. 1.0 ;

5.0 'DRIF' 7.875 0. 100. ;

APPENDIX D  
(Not optimized)  
(See Appendix J  
for  
optimal code)

(CIRCULAR DRIFT APERTURE)

16. 100. 67.7418 ;

5.0 'DRIF' 10.25 0. 100. ;

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16. 100. 70.409 ;

16. 101. 41.707 ;

5.0 'D6Q7' 27.6 9.9889 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16. 100. 67.8053 ;

16. 101. 100. ;

5.0 'DRIF' 22.1875 0.0 100. ;

7.0 'D6H6' 0.0 0.518859 0. 0. 0. 0. ;

5.0 'DRIF' 9.1875 0. 100. ;

(CIRCULAR DRIFT APERTURE)

16. 100. 69.0118 ;

5.0 'DRIF' 14.5 0. 100. ;

(CIRCULAR DRIFT APERTURE)

16. 100. 31.2928 ;

5.0 'DRIF' 2.5 0. 100. ;

(SEPTUM APERTURE)

16.0 4.0 26.035 ;

16.0 5.0 19.685 ;

2.0 0.777 ;

4.0 'ESEP' 84. 3.784 0. ;

2.0 0.777 ;

(CIRCULAR DRIFT APERTURE)

16. 100. 29.8958 ;

5.0 'DRIF' 12.8875 0. 100. ;

(SHIFT BEAM HORIZONTALLY)

7.0 115.439 0. 0. 0. 0. 0. ;

(ROTATE BEAM HORIZONTALLY.)

7.0 0. 46.99 0. 0. 0. 0. ;

(REMOVE CIRCULAR QUAD APERTURE)

16. 100. 530.937;

(HYPERBOLIC QUAD APERTURE)

16. 101. 84.1375 ;

5.0 'D6Q6' 32.6 -9.690 100. ;

(ROTATE BEAM BACK.)

7.0 0. -46.99 0. 0. 0. 0. ;

(SHIFT BEAM BACK.)

7.0 -158.75 0. 0. 0. 0. 0. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 31.039 ;

5.0 'DRIF' 11.6375 0. 100. ;

5.0 'DRIF' 188.075 0. 100. ;

(HYPERBOLIC QUAD APERTURE)

16.0 101. 41.707 ;

(CIRCULAR QUAD APERTURE)

16.0 100. 70.409 ;

5.0 'Q1' 51.64 9.8659 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16.0 100. 67.869 ;

16.0 101. 100. ;

5.0 'DRIF' 40.263 0. 100. ;

7.0 'D8V1' 0. 0. 0. 0.265646 0. 0. ;

5.0 'DRIF' 55.5125 0. 100. ;

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16.0 100. 70.409 ;

16.0 101. 41.707 ;

5.0 'Q2' 32.6 -9.0723 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16. 100. 67.869 ;

16. 101. 100. ;

5.0 'DRIF' 16.825 0. 100. ;

(CIRCULAR SEM APERTURE)

16. 100. 69.850 ;

D-2

D-3

5.0 'DRIF' 7.875 0. 100. ;  
(OBTAIN SEM 802 PROFILES)  
50. 1.0 -10. 10. 1.0 ;  
50. 3.0 -10. 10. 1.0 ;  
5.0 'DRIF' 7.875 0.0 100. ;  
(CIRCULAR DRIFT APERTURE)  
16.0 100. 67.869 ;  
5.0 'DRIF' 108.75 0. 100. ;  
7.0 'D8H4' 0. -0.040977 0. 0. 0. 0. ;  
5.0 'DRIF' 45.075 0. 100. ;  
(CIRCULAR AND HYPERBOLIC QUAD APERTURES)  
16.0 100. 70.409 ;  
16.0 101. 41.707 ;  
5.0 'Q3' 32.6 9.2759 100. ;  
(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)  
16.0 100. 67.869 ;  
16.0 101. 100. ;  
5.0 'DRIF' 24.365 0. 100. ;  
(CIRCULAR AND HYPERBOLIC QUAD APERTURES)  
16.0 100. 70.409 ;  
16.0 101. 41.707 ;  
5.0 'Q4' 27.6 -6.8517 100. ;  
(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)  
16.0 100. 67.869 ;  
16.0 101. 100. ;  
5.0 'DRIF' 122.865 0. 100. ;  
(CIRCULAR AND HYPERBOLIC QUAD APERTURES)  
16.0 100. 70.409 ;  
16.0 101. 41.707 ;  
5.0 'Q5' 32.6 7.4200 100. ;  
(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)  
16. 100. 67.742 ;  
16. 101. 100. ;  
5.0 'DRIF' 84.15 0. 100. ;  
(CIRCULAR AND HYPERBOLIC QUAD APERTURES)  
16. 100. 70.409 ;  
16. 101. 41.707 ;  
5.0 'Q6' 32.6 -7.3239 100. ;  
(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)  
16. 100. 67.742 ;  
16. 101. 100. ;  
5.0 'DRIF' 21.575 0. 100. ;  
7.0 'D8V6' 0. 0. 0. -0.198934 0. 0. ;  
5.0 'DRIF' 9.25 0. 100. ;  
(CIRCULAR DRIFT APERTURE)  
16. 100. 48.6918 ;  
5.0 'DRIF' 188.5 0. 100. ;  
(CIRCULAR DRIFT APERTURE)  
16.0 100. 67.742 ;  
(ION CHAMBER HAS BEEN REMOVED.)  
5.0 'DRIF' 13. 0. 100. ;  
(CIRCULAR DRIFT APERTURE)  
16.0 100. 67.996 ;  
5.0 'DRIF' 13.875 0. 100. ;  
(CIRCULAR SEM APERTURE)  
16.0 100. 69.850 ;  
5.0 'DRIF' 6.5 0. 100. ;  
(OBTAIN SEM 806 PROFILES.)  
50.0 1.0 -10. 10. 1. ;  
50.0 3.0 -10. 10. 1. ;  
5.0 'DRIF' 6.5 0. 100. ;  
(CIRCULAR DRIFT APERTURE)  
16.0 100. 67.996 ;  
5.0 'DRIF' 16.0 0. 100. ;  
(TB1 APERTURE)  
16.0 4.0 66.8528 ;

16.0 5.0 27.1018 ;  
20. 180. ;  
2.0 1.102 ;  
4.0 'TB1' 60. 7.48337 0. ;  
2.0 1.102 ;

D-4

(CIRCULAR DRIFT APERTURE)

16.0 100. 74.0918 ;  
5.0 'DRIF' 12.75 0. 100. ;  
2.0 1.104 ;  
4.0 'TB2' 60. 7.499 0. ;  
2.0 1.104 ;  
20. -180. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 67.1068 ;  
5.0 'DRIF' 19.575 0. 100. ;

(CIRCULAR AND HYPERBOLIC QUAD APERTURES)

16.0 100. 70.409 ;  
16.0 101. 41.707 ;  
5.0 'Q7' 18. 1.73994 100. ;

(CIRCULAR AND HYPERBOLIC DRIFT APERTURES)

16.0 100. 67.1068 ;  
16.0 101. 100. ;  
5.0 'DRIF' 9.51 0. 100. ;

(CIRCULAR TOR 807 APERTURE)

16.0 100. 28.5115 ;  
5.0 'TOR' 12. 0. 100. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 29.7688 ;  
5.0 'DRIF' 58.365 0. 100. ;

(CIRCULAR SEM APERTURE)

16.0 100. 69.85 ;  
5.0 'DRIF' 6.5 0. 100. ;

(OBTAIN SEM 807 PROFILES)

50. 1.0 -10. 10. 1. ;  
50. 3.0 -10. 10. 1. ;  
5.0 'DRIF' 6.5 0. 100. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 30.9118 ;  
5.0 'DRIF' 48.75 0. 100. ;

(SEPTUM APERTURE)

16.0 4.0 26.035 ;  
16.0 5.0 19.685 ;  
20.0 180. ;

2.0 0.859 ;  
4.0 'SEP1' 84.0 4.18526 0. ;

2.0 0.859 ;  
20.0 -180. ;

(CIRCULAR DRIFT APERTURE)

16.0 100. 31.1658 ;  
5.0 'DRIF' 3.75 0. 100. ;

20.0 180. ;  
2.0 0.822 ;  
4.0 'SEP2' 84.0 4.003 0. ;

2.0 0.822 ;  
20.0 -180. ;

5.0 'DRIF' 13.075 0. 100. ;

(SHIFT BEAM HORIZONTALLY)

7.0 -42.926 0. 0. 0. 0. ;

(CIRCULAR QUAD APERTURES)

16.0 100. 74.0918 ;

(REMOVE HYPERBOLIC QUAD APERTURES.)

16.0 101. 100. ;

5.0 'A1G4' 18.0 9.6741 100. ;

(SHIFT BEAM BACK.)

7.0 42.926 0. 0. 0. 0. ;

(OBTAIN BEAM PROFILE.)

50.0 1.0 -10. 10. 1. ;  
50.0 3.0 -10. 10. 1. ;

SENTINEL

11.22.43. UCLP, GG, TB10,

0.322KLNS.

\*\* END OF LISTING \*\*

D-5

# APPENDIX E

E,

TO: all interested parties  
FROM: R E Peters  
SUBJECT: nominal current for the 3 debuncher LQE's

Steve Holmes recently made the comment that the 3 LQE's in the debuncher at D2Q5(F), D4Q5(F), and D6Q6(D) did not appear to be as strong as expected. I believe, but am not certain, that the basis for this statement was the beta-function measurement we performed a few weeks ago.

At that time, he mentioned that the nominal current for the LQE's had been calculated from the LQD results by applying a correction factor to take into account their (slightly) different effective lengths. "New" data from MDTF indicate that the additional saturation which occurs between 1300-amperes and 1500 amperes significantly changes the predicted current.

The following table summarizes the results of some harmonic (Morsan) coil measurements.

I (amps)	INTEGRATED STRENGTH (Tesla/amp)X10**3	
1200	5.78297	<--
1250	5.71180	:
1300	5.62986	: Prototype system
1350	5.54608	:
1400	5.45629	<--
1600	5.12668	<-- MDTF

From this table we find ( $1300 \leq I \leq 1600$  amperes):

$$\text{INTEGRATED\_STRENGTH} [\times 10^{**3}] = 7.807020 * I - 1.675959E-3 * (I^{**2})$$

The nominal strength should be about 8.0 Tesla. Hence, the current be

$$\text{NOMINAL\_CURRENT} = 1522 \text{ amperes.}$$

If the present value is changed from ~1472 to 1522, the 50 ampere current increase will shift the tunes as follows:

$$D_{NUX} = +0.0117 \quad D_{NUY} = +0.003$$

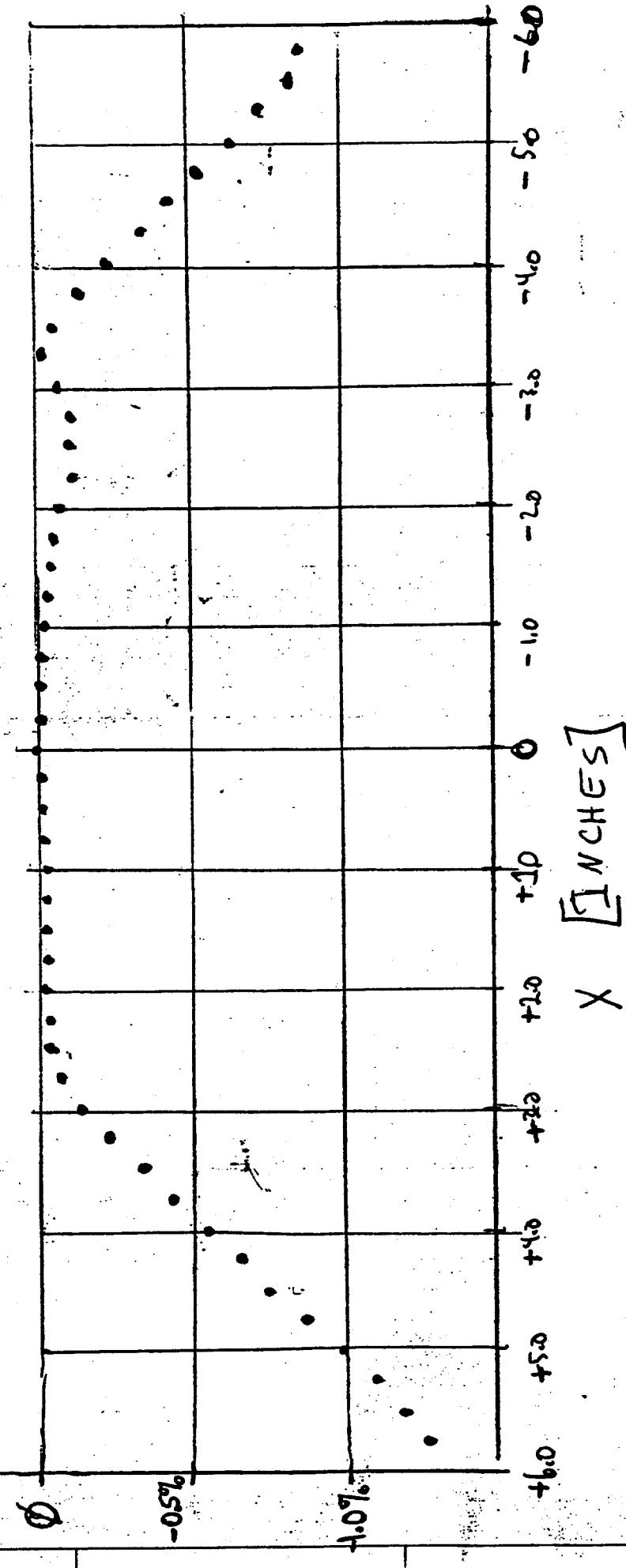
3 Sept 85

E-2

measured 5-Oct-84

0.5 in Hg

$$LQE\phi 2 \text{ at } 1600 \text{ Amp}$$
$$I = \left( \sum_{-D}^D \frac{d\beta_1(x)}{dx} dz - \sum_{-D}^D \frac{d\beta_1(\phi)}{dx} dz \right) / \sum_{-D}^D \frac{d\beta_1(k=1)}{dx} dz$$

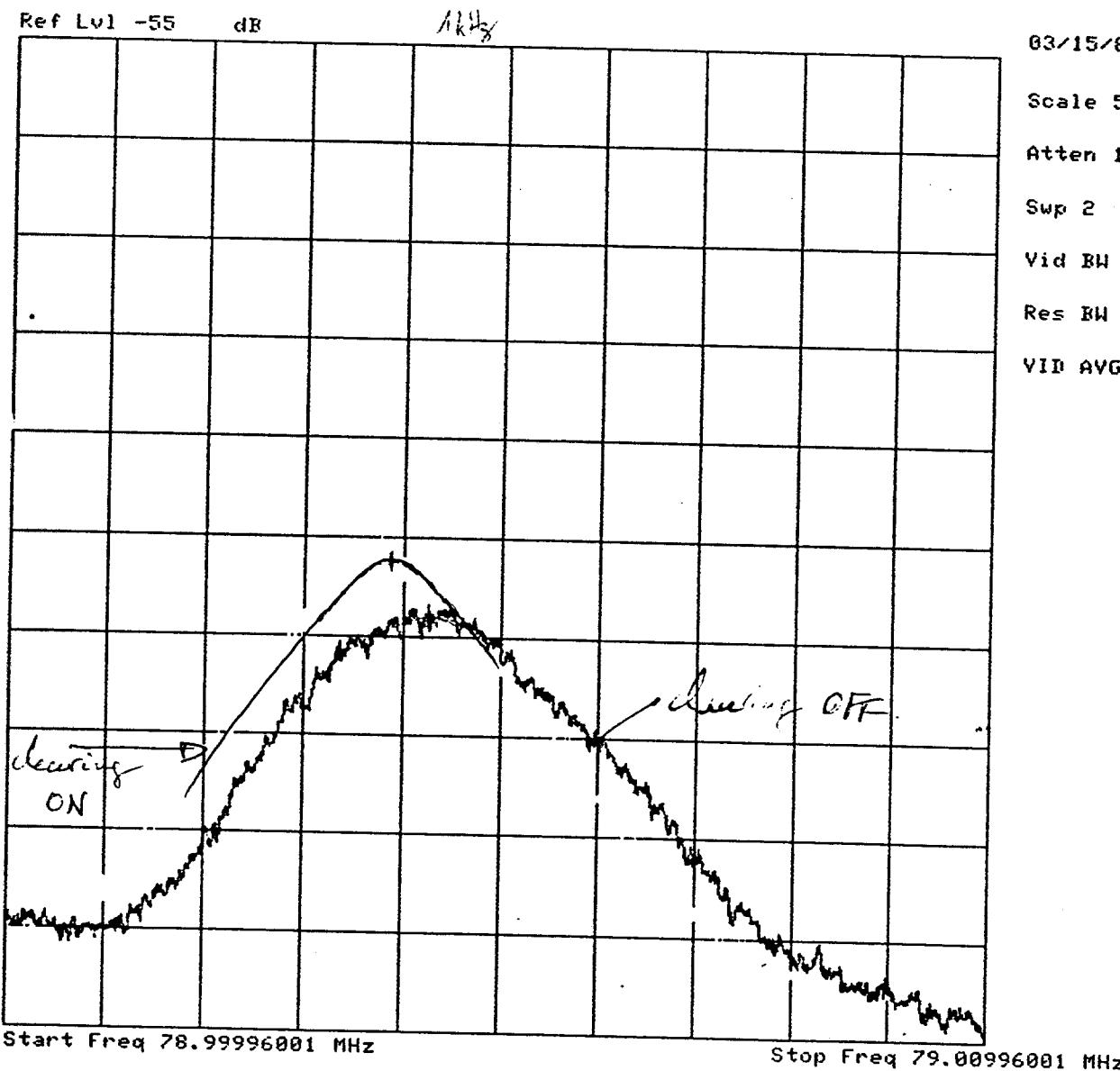


CONSOLE 08 15-MAR-1989 20:23

P28 GRAPHICS DISPLAY

ERSE blue/yellow

(A)



Vertical schottky band

$$\omega_n = (125 + Q_f) f_r$$

$$\Delta \omega_n = \Delta Q f_r$$

$$\Delta \omega_n = 400 \text{ Hz} \quad \Rightarrow \Delta Q = 6.3 \times 10^{-4}$$

## APPENDIX G

FC MAGNET ID	RUN DATE TIME	FB SLOPE	parts in ten to the fourth	FC RUN DESCRIPTION
SDD002	5-Feb-1985 23:45	-8.26E-08	+ 5.5	Normal Data Run # 2 1180.0 AMPS
SDD003	19-Oct-1984 05:44	-1.03E-06	+ 68.3	Normal Data Run # 2
SDD004	19-Oct-1984 07:15	-8.92E-07	+ 59.1	Normal Data Run # 2
SDD005	22-Oct-1984 01:45	-1.08E-06	+ 71.8	Normal Data Run # 2
SDD006	12-Oct-1984 21:53	-8.38E-07	+ 55.5	Normal Data Run ( 1230 AMPS. )
SDD007	15-Oct-1984 01:04	-1.10E-06	+ 73.0	Normal Data Run # 2
SDD008	15-Dec-1984 10:46	-9.80E-07	+ 64.9	Run # 2 Tie Plates Rewelded
SDD009	15-Oct-1984 06:00	-1.02E-06	+ 67.2	Normal Data Run # 2
SDD010	17-Dec-1984 10:20	-9.89E-07	+ 65.5	RUN # 2 TIE PLATES WELDED 1180 AMPS
SDD011	19-Dec-1984 17:29	-8.41E-07	+ 55.7	RUN # 2 TIE PLATES ARE ON 1180 AMPS MAGNET IS SHIMMED
SDD012	21-Dec-1984 13:38	-9.45E-07	+ 62.6	RUN # 2 TIE PLATES REWELDED; SHIMS ADDED 1180 AMPS
SDD013	21-Dec-1984 19:48	-8.78E-07	+ 58.1	RUN # 2 1180.0 AMPS TIE PLATES ON SHIMS ADDED
SDD014	21-Dec-1984 07:56	-9.06E-07	+ 60.0	RUN # 2 TIE PLATES WELDED 1180.0 AMPS SDD014R
SDD015	20-Dec-1984 09:25	-9.04E-07	+ 59.9	RUN # 2 TIE PLATES REWELDED; SHIMS ADDED
SDD016	6-Feb-1985 10:16	-9.54E-07	+ 63.2	RUN # 2 RETEST AFTER SITTING IN BUILDING 1180 AMPS
SDD017	17-Dec-1984 15:26	-9.99E-07	+ 66.2	RUN # 2 TIE PLATES WELDED 1180.0 AMPS SDD017R
SDD018	20-Dec-1984 17:54	-9.28E-07	+ 61.5	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD019	14-Dec-1984 10:03	-9.40E-07	+ 62.2	Run # 2 Tie Plates Rewelded
SDD020	14-Dec-1984 08:34	-7.45E-07	+ 49.3	Run # 2 Tie Plates Rewelded
SDD021	8-Dec-1984 10:43	-9.02E-07	+ 59.8	Normal Data Run # 2 After Rewelding Plates to
SDD022	20-Dec-1984 19:30	-9.11E-07	+ 60.4	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD023	19-Dec-1984 19:20	-8.76E-07	+ 58.0	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD024	20-Dec-1984 00:00	-9.59E-07	+ 63.5	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD025	13-Dec-1984 14:30	-8.80E-07	+ 58.3	RUN # 2 TIE PLATES WELDED 1180.0
SDD026	20-Dec-1984 22:08	-7.16E-07	+ 47.4	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD027	19-Dec-1984 22:15	-9.67E-07	+ 64.0	RUN # 2 1180 AMPS TIE PLATES ON SHIMS ADDED
SDD028	21-Dec-1984 15:43	-9.92E-07	+ 65.7	RUN # 2 TIE PLATES REWELDED; SHIMS ADDED
SDD029	27-Dec-1984 18:38	-9.62E-07	+ 63.7	Normal Data Run # 2 WITH TIE PLATES ON AT 1180 AMPS
SDD030	21-Dec-1984 18:12	-7.88E-07	+ 52.2	RUN # 2 TIE PLATES ON 1180.0 AMP. SHIMS ADDED
SDD031	21-Dec-1984 22:34	-7.43E-07	+ 49.2	RUN # 2 1180.0 AMPS. TIE PLATES ON SHIMS ADDED
SDD032	21-Dec-1984 10:03	-7.37E-07	+ 48.8	RUN # 2 TIE PLATES REWELDED; SHIMS ADDED
SDD033	21-Dec-1984 11:52	-7.78E-07	+ 51.5	RUN # 2 TIE PLATES WELDED 1180.0 AMPS SDD033
SDD034	3-Jan-1985 22:06	-9.27E-07	+ 61.4	RUN # 2 MAG. SHIMMED 1180 AMPS
SDD035	3-Jan-1985 08:40	-7.16E-07	+ 47.4	RUN # 2 TIE PLATES WELDED 1180 AMPS
SDD036	28-Dec-1984 13:59	-8.64E-07	+ 57.2	Run # 2 Tie Plates Welded 1180 AMPS
SDD037	4-Jan-1985 08:23	-9.68E-07	+ 64.1	RUN # 2 TIE PLATES WELDED 1180.0 AMPS
SDD038	5-Jan-1985 23:03	-8.12E-07	+ 53.7	RUN # 2 TIE PLATES AND SHIMS IN 1180.0 AMPS
SDD039	7-Jan-1985 09:23	-7.34E-07	+ 48.6	RUN # 2 TIE PLATES WELDED 1180.0 AMPS
SDD040	7-Jan-1985 15:10	-6.72E-07	+ 44.5	Normal Data Run
SDD041	7-Jan-1985 23:20	-8.88E-07	+ 58.8	RUN # 2 TIE PLATES AND SHIMS 1180.0 AMPS
SDD042	7-Jan-1985 19:15	-7.07E-07	+ 46.8	RUN # 2 TIE PLATES AND SHIMED 1180.0 AMPS
SDD043	8-Jan-1985 09:27	-8.91E-07	+ 59.0	RUN # 2 TIE PLATES REWELDED 1180 AMPS
SDD044	8-Jan-1985 14:11	-8.59E-07	+ 56.9	Run # 2 TIE PLATES REWELDED 1180 AMPS
SDD045	9-Jan-1985 11:09	-8.80E-07	+ 58.3	RUN # 2 TIE PLATES WELDED 1180.0 AMPS
SDD046	5-Feb-1985 21:31	-7.92E-07	+ 52.4	Normal Data Run # 2 1180.0 AMPS RE RUN MAGNET
SDD047	6-Feb-1985 17:23	-1.26E-06	+ 63.6	Normal Data Run # 2 1180.0 AMPS
SDD048	25-Jan-1985 14:29	-1.29E-06	+ 65.6	RUN # 2 ALPHA STEEL 1180.0 AMPS
SDD049	26-Jan-1985 21:51	-1.12E-06	+ 74.4	RUN # 2 TIE PLATES ON 1180.0 AMPS
SDD050	30-Jan-1985 14:36	-9.46E-07	+ 62.7	RUN # 2 LAYERED CAKE RECIPE 1180 AMPS
SDD051	31-Jan-1985 14:47	-9.67E-07	+ 64.0	RUN # 2 LAYERED CAKE RECIPE 1180 AMPS
SDD052	1-Feb-1985 08:12	-9.24E-07	+ 61.2	RUN # 2 LAYERED CAKE RECIPE 1180 AMPS BY BETTY CROCI
SDD053	1-Feb-1985 15:30	-6.37E-07	+ 42.2	RUN # 2 LAYERED CAKE RECIPE 1180 AMPS PILLSBURY
SDD054	4-Feb-1985 12:55	-7.02E-07	+ 46.5	RUN # 2 LAYERED RECIPE 1180 AMPS
SDD055	4-Feb-1985 21:24	-7.71E-07	+ 51.0	LAYER CAKE RUN # 2 1180.0 AMPS
SDD056	4-Feb-1985 17:26	-8.11E-07	+ 53.7	Normal Data Run # 2 1180.0 AMPS
SDD057	5-Feb-1985 14:58	-6.74E-07	+ 44.6	RUN # 2 RECIPE LAYER MAGNET 1180 AMPS
SDD058	5-Feb-1985 11:15	-7.43E-07	+ 49.2	RUN # 2 RECIPE MAGNET 1180 AMPS
SDD059	6-Feb-1985 12:23	-8.59E-07	+ 56.9	RUN # 2 LAYERED RECIPE @1180 AMPS.
SDD060	6-Feb-1985 14:19	-9.15E-07	+ 60.6	RUN # 2 RECIPE FORMULA 1180 AMPS
SDD061	7-Feb-1985 10:49	-9.51E-07	+ 63.0	RUN # 2 RECIPE MAGNET 1180 AMPS
SDD062	7-Feb-1985 14:55	-9.95E-07	+ 65.9	RUN # 2 RECIPE MAG 1180.0 AMPS
SDD063	11-Feb-1985 09:39	-6.59E-07	+ 43.7	RUN # 2 RECIPE MAGNET 1180.0 AMPS
SDD064	8-Feb-1985 10:42	-9.54E-07	+ 63.2	RUN # 2 RECIPE MAGNET 1180 AMPS
SDD065	11-Feb-1985 14:20	-1.01E-06	+ 66.7	RUN # 2 RECIPE 1180 AMPS
SDD066	11-Feb-1985 16:46	-1.25E-06	+ 62.6	Normal Data Run # 2 @ 1180.0 AMP 1180 AMPS
SDD067	11-Feb-1985 12:48	-1.22E-06	+ 81.1	RUN # 2 RECIPE 1180 AMPS
SDD068	11-Feb-1985 19:13	-1.24E-06	+ 81.7	Normal Data Run RUN # 2 @ 1180.0 AMP
SDD069	11-Feb-1985 22:05	-1.11E-06	+ 73.6	Normal Data Run # 2 @ 1180.0 AMP
SDD070	5-Jan-1985 17:42	-5.86E-07	+ 38.8	Normal Data Run # 2 1180.0 AMPS

# APPENDIX H

H-1

Single Probe

$$V = \frac{BA}{RC}$$

$$\frac{1}{RC} = 1000, A = .11'' \times 80'' = .00568 \text{ m}^2$$

<u><math>V_c</math></u>	<u><math>V_{peak}</math></u>	<u><math>B_{peak}</math></u> (kG)
250.3	$1.388 \pm .03$	$2.444 \pm .053$
350.1	$1.955$	$3.442$
449.1	$2.490$	$4.384$
549.2	$3.040$	$5.352$
620.1	$3.420$	$6.021$

$$\frac{1}{RC} = 100000, V_{peak} = .040 \pm .01 \Rightarrow B_{peak} = 0.7 \text{ Gauss}$$

Septum Excitation Data



FERMILAB

## ENGINEERING NOTE

SECTION

PROJECT

SERIAL-CATEGORY

H-1

SUBJECT

NAME

Septum Field Measurements

DATE

REVISION DATE

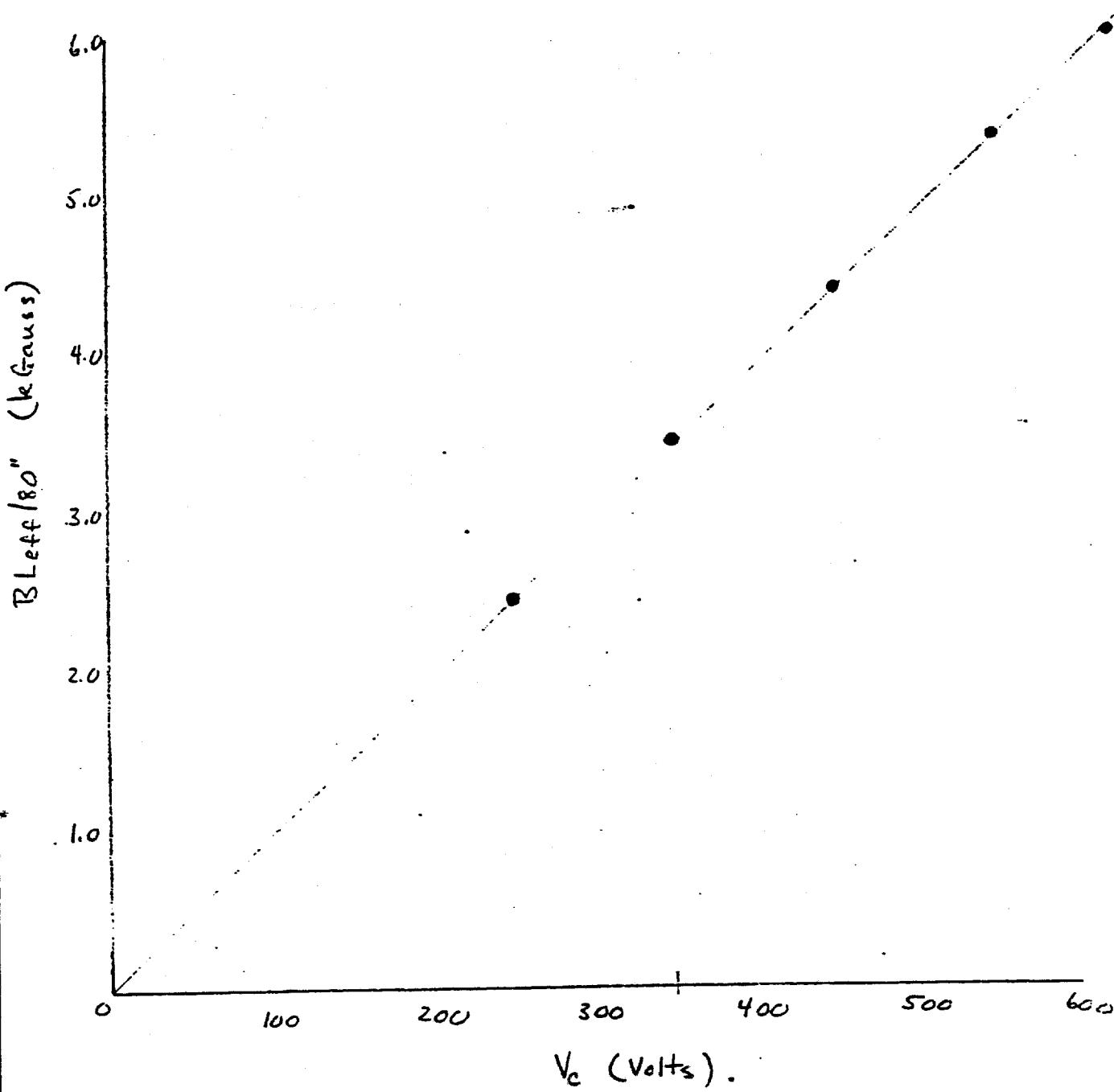


Figure 1

# APPENDIX I

## ~~APPENDIX I~~ KICKER DATA

	DEBUNCHER PROTON	DEBUNCHER ANTIPROTON				
PARAMETER	INJECTION	INJECTION	DEBUNCHER EXTRACTION	ACCUMULATOR INJECTION	ACCUMULATOR EXTRACTION	UNITS
FIELD RISE TIME			190		225	ns
FIELD FALL TIME	205	205		75		ns
PULSE WIDTH min	1.49	1.49	1.505	1.505	0.25	us
PFN LENGTH min	1.695	1.695	1.695	1.58	0.475	us
TOTAL KICK NEEDED	6.1	6.1	4.6	4	4	us
BEAM ENERGY	8	8	8	8	8	GeV
DEFLECTION	10	10	6	6.5	6.5	mm
DIRECTION	VERTICAL	VERTICAL	HORIZONTAL	HORIZONTAL	HORIZONTAL	
$\int B \cdot dI$	1810	1810	1340	1190	1190	gauss-meters
MAGNETIC LENGTH	2.77	2.77	2.34	2.24	2.24	meters
FIELD NEEDED	650	650	574	531	531	gauss
APERTURE (WxH)	56x42	56x42	42x75	30.5x250	30.5x250	mm
BEAM SIZE	32x32	32x32	35x64	25x52	25x52	mm
FERRITE GAP SIZE	65x50	65x50	52x84	30.5x57	30.5x57	mm
FERRITE TYPE	CMD 5005	CMD 5005	CMD 5005	4C6	4C6	
IMPEDANCE	10	10	12.5	23	23	$\Omega$
CURRENT	2530	2530	2420	1400	1400	Amps
VOLTAGE	25.3	25.3	30.2	35	35	kV
* OF MAGNETS	3	3	3	3	3	
INDUCTANCE	1.52	1.52	1.55	1.73	1.73	uH
TOTAL CAPACITANCE	15200	15200	9920	2768	2768	pF
* OF "T" CELLS	12	12	10	9	9	
PROP. DELAY	150	150	125	62	62	ns
FLANGE TO FLANGE	125.125	125.125	107.875	122.8025	122.8025	inches
LOCATION	D202	D402	D609	A20	A20	

7-2

Page 3

## CERAMIC TUBES - ALL TYPES USED

DATE: 12/21/84

<b>SIZE &amp; SHAPE</b>	1-5/8" x 2-1/4" ID ELLIPSE 41" LONG	1-3/4" x 3" ID ELONG. ELLIPSE 35" LONG	2-3/4" O.D. x 2-1/2" I.D. ROUND 45" LONG	5-1/4" O.D. x 4-7/8" I.D. LG. ROUND 60" LONG
<b>DRAWING NUMBER</b>	1751 - MC - 139750	1751 - MC - 139751	1751 - MD - 139851	OBsolete
<b>FABRICATION LABELS</b>	B(41")E	$\Sigma$ (35")EE	R(45")	RL(BO")
<b>RAW TUBES ON ORDER</b>	0	0	0	0
<b>TUBES UNFLANGED / W # I.D.</b>	3 # B - 10, 11, 12	3 # L - 6, 7, 8	2 - 48" Long 3 - 45" Long	4 # R <sub>L</sub> - 3, 4, 5, 6 X-GAL
<b>TUBES FLANGED / W # I.D.</b>	9 # B - 1, 2, 3, 4, 5, 6, 7, 8, 9	5 # L - 1, 2, 3, 4, 5	4 R - 3(45") R - 6 (45") * R - 3(45") R - 5 (45")	2 # R <sub>L</sub> - 1, 2 } New Tubes
<b>TUBES FLANGED &amp; COATED / W # I.D., RESISTANCE F.F., STORAGE LOCATION</b>	0	0	0	0
<b># TUBES TO BE INSTALLED / MAGNET APPLICATION</b>	6 and 1 Spare	3 and 1 Spare	2 => 1 Set and 1 Spare Set	0
<b># TUBES / MAGNETS IN OPERATION TUNNEL LOCATION</b>	Debuncher Injection	Debuncher Extraction	Booster Fast Kicker (L-2)	Proposed Horiz. Injection
<b>BAD TUBES . (STATUS)</b>	<i>AVERAGE WALL THICKNESS</i> <i>1/8"</i>			1 Broken ≈ 36" usable - no flanges 2 Leaks Flange (HOT)
TFS: (1) DIMENSIONS GIVEN ARE ACTUAL DIMENSIONS				

"DEBUNCHER TO ACCUMULATOR TRANSFER LINE  
(STARTING JUST US OF D6Q10 AND ENDING JUST DS OF A1Q4  
(FEBRUARY 5, 1993

HCPENND-X

J-1

1. 000000	2. 522700	. 46200	-4. 11500	. 28400	9332. 00000	. 10000
(LINE BEGINS JUST UPSTREAM OF D6Q10.						
16. 00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	100. 00000	70. 40900,			
16. 00	101. 00000	41. 70700,				
16. 00	"D010"	27. 60000	-7. 74380	100. 00000,		
16. 00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	100. 00000	67. 80530,			
16. 00	101. 00000	100. 00000,	67. 80530,			
16. 00	"DRIF"	20. 12750	0. 00000,	100. 00000,		
16. 00	(CIRCULAR DRIFT APERTURE	100. 00000	48. 69180,			
16. 00	"DRIF"	4. 75000	0. 00000,	100. 00000,		
16. 00	(EKIK APERTURE	4. 00000	38. 10000,			
16. 00	"DRIF"	5. 00000	22. 22500,			
16. 00	"EKIK"	98. 37500	. 53600	0. 00000,		
2. 0	(CIRCULAR DRIFT APERTURE	12900,				
4. 000	"DRIF"	100. 00000	48. 60270,			
5. 00	(CIRCULAR DRIFT APERTURE	4. 75000	0. 00000,	100. 00000,		
16. 00	"DRIF"	100. 00000	48. 12280,			
5. 00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	16. 89750	0. 00000,	100. 00000,		
16. 00	100. 00000	70. 40900,				
16. 00	"D607"	101. 00000	41. 70700,			
5. 00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	27. 60000	9. 98890	100. 00000,		
16. 00	100. 00000	67. 74180,				
16. 00	"DRIF"	101. 00000	100. 00000,			
5. 00	D6BS APERTURE	40. 76400	0. 00000,	100. 00000,		
16. 00	"DRIF"	4. 00000	78. 85430,			
16. 00	"DRIF"	5. 00000	26. 86370,			
2. 0	"DRIF"	2. 70880,				
4. 000	"D68B"	65. 37000	16. 93780	0. 00000,		
2. 0	"DRIF"	2. 70880,				
5. 00	"DRIF"	40. 76000	0. 00000	100. 00000,		
16. 00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	100. 00000	70. 40900,			
16. 00	101. 00000	41. 70700,				
16. 00	"D6GB"	27. 60000	-9. 74380	100. 00000,		
5. 00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	100. 00000	47. 74180,			
16. 00	101. 00000	100. 00000,	47. 74180,			
5. 00	"DRIF"	40. 76000	0. 00000	100. 00000,		
2. 0	"DRIF"	2. 72970,				
4. 000	"D6B7"	65. 37000	17. 05850	0. 00000,		
5. 00	"DRIF"	2. 72970,				
16. 00	CIRCULAR BEM APERTURE	14. 76000	0. 00000	100. 00000,		
5. 00	"DRIF"	100. 00000	49. 85000,	0. 00000	100. 00000,	
50. 0	OBTAIN SEM 607 PROFILES	7. 87500	0. 00000	100. 00000,		
50. 0	"DRIF"	3. 00000	-10. 00000	10. 00000	1. 00000,	
5. 00	"DRIF"	7. 87500	0. 00000	100. 00000,		

J-2

1	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	100.00000	67.74180!	
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	5.00	"DRIF"	10.28000	0.00000	100.00000,
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	16.00	"DRIF"	100.00000	70.40900!	
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	16.00	"DRIF"	101.00000	41.70700!	
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	5.00	"D607"	27.68000	9.98890	100.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	16.00	"DRIF"	100.00000	67.80530!	
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	16.00	"DRIF"	101.00000	100.00000!	
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"DRIF"	22.18750	0.00000!	100.00000!
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	7.00	"D6H6"	0.00000	51886	0.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"DRIF"	9.18750	0.00000	100.00000,
	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	100.00000	69.01180!	
	(CIRCULAR DRIFT APERTURE	5.00	"DRIF"	14.58000	0.00000	100.00000,
	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	100.00000	31.29280!	
	(CIRCULAR DRIFT APERTURE	5.00	"DRIF"	2.58000	0.00000	100.00000,
	(BEPTUM APERTURE	16.00	"EBEP"	4.00000	26.03500!	
	(BEPTUM APERTURE	16.00	"EBEP"	5.00000	19.68500!	
	(BEPTUM APERTURE	2.0	"EBEP"	7.77000	3.78400	0.00000,
	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	100.00000	29.89580!	
	(CIRCULAR DRIFT APERTURE	5.00	"DRIF"	12.98750	0.00000	100.00000!
	(SHIFT BEAM HORIZONTALLY	7.0	"ROTATE BEAM HORIZONTALLY	122.43890	0.00000	0.00000,
	(REMOVE CIRCULAR QUAD APERTURE	7.0	"ROTATE BEAM BACK,	0.00000	42.00000	0.00000,
	(HYPERBOLIC QUAD APERTURE	16.00	"D606"	100.00000	530.93700!	
	(HYPERBOLIC QUAD APERTURE	16.00	"D606"	101.00000	84.13750!	
	(ROTATE BEAM BACK,	5.00	"ROTATE BEAM BACK,	32.46000	-9.69000	100.00000,
	(SHIFT BEAM BACK,	7.0	"ROTATE BEAM BACK,	0.00000	-88.00000	0.00000,
	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	-170.38000	0.00000	0.00000,
	(CIRCULAR DRIFT APERTURE	16.00	"DRIF"	100.00000	31.03900!	
	(CIRCULAR DRIFT APERTURE	5.00	"DRIF"	11.63750	0.00000	100.00000,
	(CIRCULAR DRIFT APERTURE	50.0	"DRIF"	1.00000	-40.00000	40.00000,
	(CIRCULAR DRIFT APERTURE	50.0	"DRIF"	3.00000	-10.00000	10.00000,
	(CIRCULAR DRIFT APERTURE	5.00	"DRIF"	188.07500	0.00000	100.00000,
	(CIRCULAR DRIFT APERTURE	50.0	"DRIF"	1.00000	-40.00000	40.00000,
	(CIRCULAR DRIFT APERTURE	50.0	"DRIF"	3.00000	-10.00000	10.00000,
	(HYPERBOLIC QUAD APERTURE	16.00	"DRIF"	101.00000	41.70700!	
	(CIRCULAR QUAD APERTURE	16.00	"Q1"	100.00000	70.40900!	
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"Q1"	91.64000	9.86590	100.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	16.00	"DRIF"	101.00000	67.86900!	
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"DRIF"	40.26300	0.00000	100.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	7.0	"DSV1"	0.00000	0.00000	0.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"DRIF"	55.31250	0.00000	100.00000,
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	16.00	"DRIF"	100.00000	70.40900!	
	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	16.00	"Q2"	101.00000	41.70700!	
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	5.00	"Q2"	32.46000	-9.07230	100.00000,
	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	16.00	"DRIF"	100.00000	67.86900!	

(See J-6)  
below

J-3

16.00	"DRIF"	101.00000	100.00000	100.00000	100.00000	)
5.00	(CIRCULAR SEM APERTURE	16.82500	0.00000	0.00000	0.00000	)
16.00	"DRIF"	100.00000	69.85000	100.00000	100.00000	)
5.00	(OBTAIN SEM 802 PROFILES	7.87500	0.00000	0.00000	0.00000	)
50.0	50.0	50.0	50.0	50.0	50.0	)
5.00	"DRIF"	1.00000	-10.00000	10.00000	10.00000	)
16.00	"DRIF"	3.00000	-10.00000	10.00000	10.00000	)
5.00	(CIRCULAR DRIFT APERTURE	7.87500	0.00000	0.00000	0.00000	)
16.00	"DRIF"	100.00000	67.86900	100.00000	100.00000	)
5.00	"DBH4"	108.75000	0.00000	0.00000	0.00000	)
7.	"DRIF"	45.07500	0.00000	0.00000	0.00000	)
5.00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	45.07500	0.00000	0.00000	0.00000	)
16.00	"DRIF"	100.00000	70.40900	100.00000	100.00000	)
16.00	"Q3"	101.00000	71.70700	101.00000	101.00000	)
5.00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	32.60000	9.27590	100.00000	100.00000	)
16.00	"DRIF"	100.00000	67.86900	100.00000	100.00000	)
16.00	"DRIF"	101.00000	100.00000	100.00000	100.00000	)
5.00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	24.35000	0.00000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	70.40900	100.00000	100.00000	)
16.00	"Q4"	101.00000	71.70700	101.00000	101.00000	)
5.00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	27.60000	-6.85170	100.00000	100.00000	)
16.00	"DRIF"	100.00000	67.86900	100.00000	100.00000	)
16.00	"Q5"	101.00000	100.00000	100.00000	100.00000	)
5.00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	32.60000	7.42000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	67.74200	100.00000	100.00000	)
16.00	"DRIF"	101.00000	100.00000	100.00000	100.00000	)
5.00	(CIRCULAR AND HYPERBOLIC QUAD APERTURES	84.15000	0.00000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	70.40900	100.00000	100.00000	)
16.00	"Q6"	101.00000	71.70700	101.00000	101.00000	)
5.00	(CIRCULAR AND HYPERBOLIC DRIFT APERTURES	32.60000	-7.32390	100.00000	100.00000	)
16.00	"DRIF"	100.00000	67.74200	100.00000	100.00000	)
16.00	"DBV6"	101.00000	100.00000	100.00000	100.00000	)
7.	"DRIF"	21.57500	0.00000	100.00000	100.00000	)
5.00	(CIRCULAR DRIFT APERTURE	9.25000	0.00000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	48.69180	100.00000	100.00000	)
5.00	(CIRCULAR DRIFT APERTURE	168.50000	0.00000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	67.74200	100.00000	100.00000	)
5.00	(CIRCULAR SEM APERTURE	13.87500	0.00000	100.00000	100.00000	)
16.00	"DRIF"	100.00000	69.85000	100.00000	100.00000	)
5.00	(CIRCULAR DRIFT APERTURE	6.50000	0.00000	100.00000	100.00000	)
50.0	(OBTAIN SEM 802 PROFILES	1.00000	-25.00000	25.00000	25.00000	)
50.0	"DRIF"	3.00000	-20.00000	20.00000	20.00000	)
5.00	(CIRCULAR DRIFT APERTURE	4.50000	0.00000	100.00000	100.00000	)

J-4

16.00	5.00	"DRIF"	100.00000	67.99600,	100.00000,
(TB1 APERTURE			16.00000	0.00000	100.00000,
16.00	5.00	"DRIF"	4.00000	66.85260,	
16.00	5.00000		5.00000	27.10180,	
20.0	2.0		180.00000,		
2.0	4.000	"TB1 "	1.10200,	7.48337	0.00000,
2.0	4.000	"TB2 "	60.00000		
2.0	2.0		1.10400,	7.49900	0.00000,
20.0	2.0		-180.00000,		
(CIRCULAR DRIFT APERTURE			100.00000	74.09180,	
16.00	5.00	"DRIF"	12.75000	0.00000	100.00000,
2.0	4.000	"TB2 "	1.10400,		
2.0	2.0		60.00000		
20.0	2.0		1.10400,		
(CIRCULAR DRIFT APERTURE			100.00000	67.10680,	
16.00	5.00	"DRIF"	19.97500	0.00000	100.00000,
(CIRCULAR AND HYPERBOLIC QUAD APERTURES			100.00000	70.40900,	
16.00	16.00		101.00000	41.70700,	
16.00	5.00	"007 "	18.00000	1.73994	100.00000,
(CIRCULAR AND HYPERBOLIC DRIFT APERTURES			100.00000	67.10680,	
16.00	16.00	"DRIF"	101.00000	100.00000,	
16.00	5.00	"DRIF"	1.9.51000	0.00000	100.00000,
(CIRCULAR TCR 807 APERTURE			100.00000	28.91150,	
16.00	5.00	"TCR "	12.00000	0.00000	100.00000,
(CIRCULAR DRIFT APERTURE			100.00000	29.76800,	
16.00	5.00	"DRIF"	98.36300	0.00000	100.00000,
(CIRCULAR BEH APERTURE			100.00000	69.85000,	
16.00	5.00	"DRIF"	4.50000	0.00000	100.00000,
(OBTAIN BEH 807 "PROFILES			1.00000	-25.00000	25.00000,
50.0	50.0	"DRIF"	3.00000	-10.00000	10.00000,
(CIRCULAR DRIFT APERTURE			6.50000	0.00000	100.00000,
16.00	5.00	"DRIF"	100.00000	30.91180,	
(SEPTUM APERTURE			48.75000	0.00000	100.00000,
16.00	16.00	"SEPT1"	4.00000	26.03500,	
20.0	2.0		5.00000	19.68500,	
2.0	4.000		180.00000,		
2.0	2.0		83900,		
20.0	2.0		84.00000	4.18926	0.00000,
(CIRCULAR DRIFT APERTURE			-180.00000,		
16.00	5.00	"DRIF"	100.00000	31.16580,	
20.0	2.0		3.75000	0.00000	100.00000,
2.0	4.000	"SEP2"	180.00000,		
2.0	2.0		82200,		
20.0	2.0		82200,	4.00300	0.00000,
(SHIFT BEAM HORIZONTALLY			-180.00000		
7.			13.07500	0.00000	100.00000,
(CIRCULAR QUAD APERTURES			-42.92600	0.00000	0.00000
16.00			100.00000	74.09180,	
(REMOVE HYPERBOLIC QUAD APERTURES.			101.09000	100.00000,	

J-5

5.00 "A104" 18.00000 9.67410 100.00000  
SHIFT BEAM BACK.  
7.00000 42.92600 0.00000 0.00000 0.00000 0.00000,  
(OBTAIN BEAM PROFILE.  
50.0 1.00000 -30.00000 30.00000 2.00000;  
50.0 3.00000 -10.00000 10.00000 1.00000;

OSSENTINEL  
1 DEBUNCHER TO ACCUMULATOR TRANSFER LINE  
\*\*\*\*\* FOLLOWING HISTOGRAMS REFER TO 1000 RAYS PASSING THROUGH THE ABOVE BEAM LINE  
\*\*\*\*\* FOLLOWING HISTOGRAMS HAVE BEEN REQUESTED

HISTOGRAM NO 1  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 2  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 3  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 4  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 5  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 6  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 7  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 8  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 9  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 10  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 11  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 12  
DISTRIBUTION OF Y IN MM  
HISTOGRAM NO 13  
DISTRIBUTION OF X IN MM  
HISTOGRAM NO 14  
DISTRIBUTION OF Y IN MM  
0 19658 PLACES LEFT FOR HISTOGRAM STORAGE  
1 HISTOGRAM NO 1  
DISTRIBUTION OF X IN MM  
0 LESS THAN -10.000 0  
-10.000 TO -9.000 0  
-9.000 TO -8.000 0  
-8.000 TO -7.000 0  
-7.000 TO -6.000 14  
-6.000 TO -5.000 119  
-5.000 TO -4.000 340  
-4.000 TO -3.000 708  
-3.000 TO -2.000 974  
-2.000 TO -1.000 1352  
-1.000 TO 0.000 1483  
0.000 TO 1.000 1522  
1.000 TO 2.000 1318  
2.000 TO 3.000 1062  
3.000 TO 4.000 672  
4.000 TO 5.000 313  
5.000 TO 6.000 111  
6.000 TO 7.000 12  
7.000 TO 8.000 0  
8.000 TO 9.000 0

505.359 IN FROM THE TARGET

505.359 IN FROM THE TARGET

740.584 IN FROM THE TARGET

740.584 IN FROM THE TARGET

928.659 IN FROM THE TARGET

928.659 IN FROM THE TARGET

1133.375 IN FROM THE TARGET

1133.375 IN FROM THE TARGET

1904.554 IN FROM THE TARGET

2183.754 IN FROM THE TARGET

2183.754 IN FROM THE TARGET

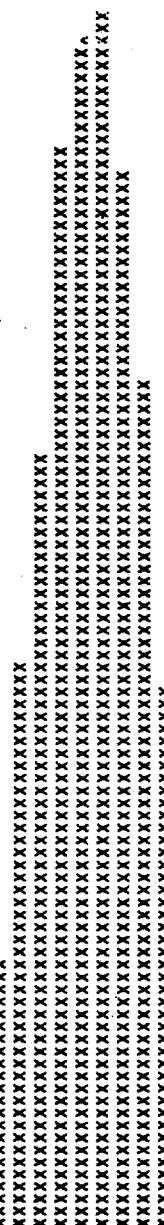
2441.829 IN FROM THE TARGET

2441.829 IN FROM THE TARGET

505.359 IN FROM THE TARGET

SCALE FACTOR. 100 X'S EQUAL 1522 ENTRIES

SEM 607



T-6

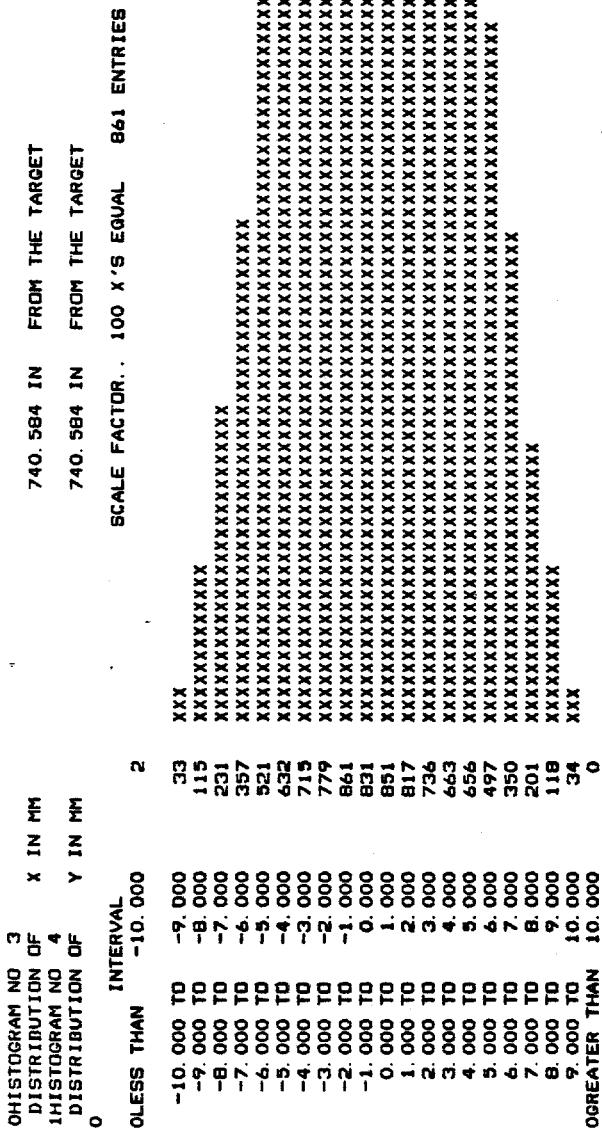
SEM 607

GREATER THAN 10.000		0		INCLUDING UNDERFLOW AND OVERFLOW	
0	TOTAL NUMBER OF ENTRIES =	10000	RMS HALF WIDTH =	2. 381	
	CENTER =	. 011			
HISTOGRAM NO 1	DISTRIBUTION OF X IN MM				
HISTOGRAM NO 2	DISTRIBUTION OF Y IN MM				
0	LESS THAN INTERVAL	-10.000	0		
-10. 000 TO -9. 000	-9. 000 TO -8. 000	0	0		
-8. 000 TO -7. 000	-7. 000 TO -6. 000	0	0		
-6. 000 TO -5. 000	-5. 000 TO -4. 000	130	367		
-4. 000 TO -3. 000	-3. 000 TO -2. 000	689	1073		
-2. 000 TO -1. 000	-1. 000 TO 0. 000	1321	1494		
0. 000 TO 1. 000	1. 000 TO 2. 000	1480	1253		
1. 000 TO 2. 000	2. 000 TO 3. 000	1029	676		
3. 000 TO 4. 000	4. 000 TO 5. 000	349	349		
5. 000 TO 6. 000	6. 000 TO 7. 000	123	9		
7. 000 TO 8. 000	8. 000 TO 9. 000	0	0		
9. 000 TO 10. 000	0	0	0		
GREATER THAN 10.000		0		INCLUDING UNDERFLOW AND OVERFLOW	
0	TOTAL NUMBER OF ENTRIES =	10000	RMS HALF WIDTH =	2. 414	
	CENTER =	. 039			
HISTOGRAM NO 2	DISTRIBUTION OF Y IN MM				
HISTOGRAM NO 3	DISTRIBUTION OF X IN MM				
0	LESS THAN INTERVAL	-40. 000	0		
-40. 000 TO -36. 000	-36. 000 TO -32. 000	0	0		
-32. 000 TO -28. 000	-28. 000 TO -24. 000	0	0		
-24. 000 TO -20. 000	-20. 000 TO -16. 000	0	0		
-16. 000 TO -12. 000	-12. 000 TO -8. 000	0	0		
-8. 000 TO -4. 000	-4. 000 TO 0. 000	267	8456		
0. 000 TO 4. 000	4. 000 TO 8. 000	1277	1277		
8. 000 TO 12. 000	12. 000 TO 16. 000	0	0		
16. 000 TO 20. 000	20. 000 TO 24. 000	0	0		
24. 000 TO 28. 000	28. 000 TO 32. 000	0	0		
32. 000 TO 36. 000	36. 000 TO 40. 000	0	0		
40. 000 TO 40. 000	0	0	0		
GREATER THAN 40.000		0		INCLUDING UNDERFLOW AND OVERFLOW	
0	TOTAL NUMBER OF ENTRIES =	10000	RMS HALF WIDTH =	1. 297	
	CENTER =	2. 451			

Just before  
188" drift marked  
with asterisk above

J-7

Just  
before 188" drift



Just after  
the 188" drift

0            INTERVAL      OLESS THAN -10. 000      0  
 -10. 000 TO -9. 000      0  
 -9. 000 TO -8. 000      0  
 -8. 000 TO -7. 000      0  
 -7. 000 TO -6. 000      0  
 -6. 000 TO -5. 000      0  
 -5. 000 TO -4. 000      0  
 -4. 000 TO -3. 000      0  
 -3. 000 TO -2. 000      0  
 -2. 000 TO -1. 000      0  
 -1. 000 TO 0. 000      0  
 0. 000 TO 1. 000      0  
 1. 000 TO 2. 000      0  
 2. 000 TO 3. 000      0  
 3. 000 TO 4. 000      0  
 4. 000 TO 5. 000      0  
 5. 000 TO 6. 000      0  
 6. 000 TO 7. 000      0  
 7. 000 TO 8. 000      0  
 8. 000 TO 9. 000      0  
 9. 000 TO 10. 000      0  
 OGREATERTHAN 10. 000      0  
 0            TOTAL NUMBER OF ENTRIES = 9836      RMS HALF WIDTH = .860      INCLUDING UNDERFLOW AND OVERFLOW  
 OHISTOGRAM NO 6      CENTER = -.013  
 DISTRIBUTION OF Y IN MM  
 IHISTOGRAM NO 7  
 DISTRIBUTION OF X IN MM  
 0            INTERVAL      OLESS THAN -10. 000      0  
 -10. 000 TO -9. 000      0  
 -9. 000 TO -8. 000      63      X  
 -8. 000 TO -7. 000      935      XXXXXXXXXXXXXXXXXXXXXXX  
 -7. 000 TO -6. 000      2431      XXXXXXXXXXXXXXXXXXXXXXX  
 -6. 000 TO -5. 000      32253      XXXXXXXXXXXXXXXXXXXXXXX  
 -5. 000 TO -4. 000      2316      XXXXXXXXXXXXXXXXXXXXXXX  
 -4. 000 TO -3. 000      814      XXXXXXXXXXXXXXXXXXXXXXX  
 -3. 000 TO -2. 000      24  
 -2. 000 TO -1. 000      0  
 -1. 000 TO 0. 000      0  
 0. 000 TO 1. 000      0  
 1. 000 TO 2. 000      0  
 2. 000 TO 3. 000      0  
 3. 000 TO 4. 000      0  
 4. 000 TO 5. 000      0  
 5. 000 TO 6. 000      0  
 6. 000 TO 7. 000      0  
 7. 000 TO 8. 000      0  
 8. 000 TO 9. 000      0  
 9. 000 TO 10. 000      0  
 OGREATERTHAN 10. 000      0  
 0            TOTAL NUMBER OF ENTRIES = 9836      RMS HALF WIDTH = 1. 090      INCLUDING UNDERFLOW AND OVERFLOW  
 OHISTOGRAM NO 7      CENTER = -.547  
 DISTRIBUTION OF X IN MM  
 IHISTOGRAM NO 6  
 DISTRIBUTION OF Y IN MM  
 0            INTERVAL      OLESS THAN -10. 000      0

SCALE FACTOR.. 100 X'S EQUAL 3490 ENTRIES

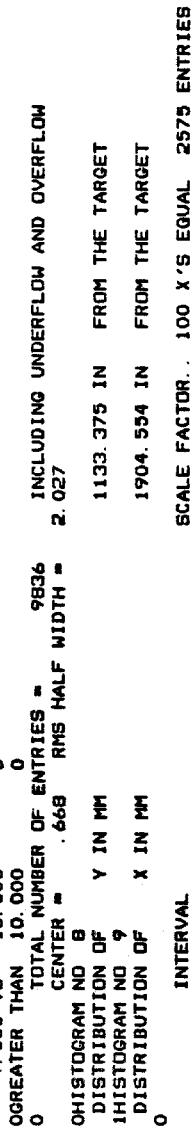
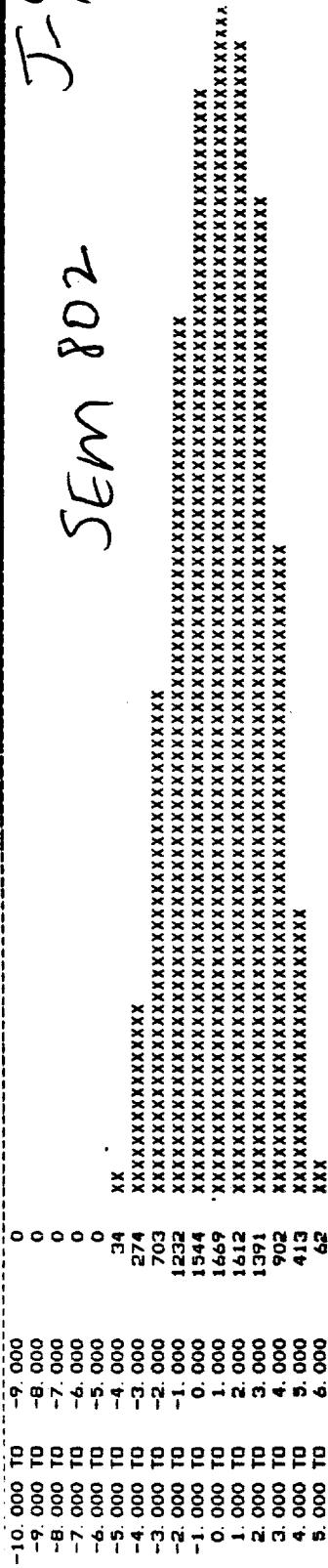
Just after 188" drift

J-8  
Sem 802

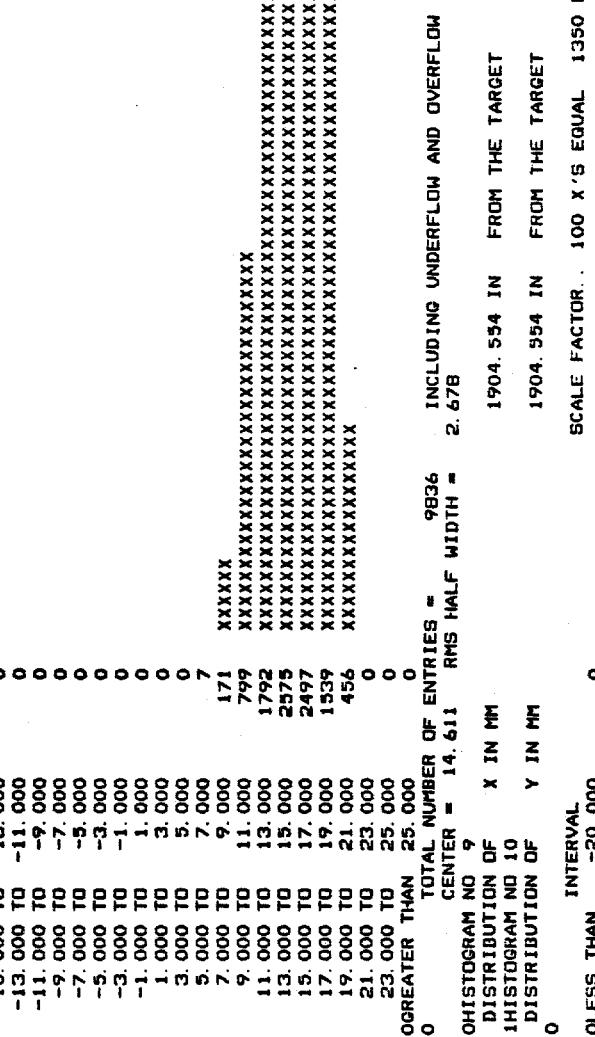
1133. 375 IN FROM THE TARGET  
 1133. 375 IN FROM THE TARGET  
 SCALE FACTOR.. 100 X'S EQUAL 3253 ENTRIES  
 928. 659 IN FROM THE TARGET  
 1133. 375 IN FROM THE TARGET  
 SCALE FACTOR.. 100 X'S EQUAL 3253 ENTRIES  
 1133. 375 IN FROM THE TARGET  
 1133. 375 IN FROM THE TARGET  
 SCALE FACTOR.. 100 X'S EQUAL 1669 ENTRIES

J-9

SEM 802



SEM 806



-20. 000 TO -18. 000 0  
 -18. 000 TO -16. 000 0  
 -16. 000 TO -14. 000 0  
 -14. 000 TO -12. 000 0  
 -12. 000 TO -10. 000 55  
 -10. 000 TO -8. 000 189  
 -8. 000 TO -6. 000 401  
 -6. 000 TO -4. 000 661  
 -4. 000 TO -2. 000 968  
 -2. 000 TO 0. 000 1108  
 0. 000 TO 2. 000 1280  
 2. 000 TO 4. 000 1350  
 4. 000 TO 6. 000 1230  
 6. 000 TO 8. 000 983  
 8. 000 TO 10. 000 789  
 10. 000 TO 12. 000 496  
 12. 000 TO 14. 000 242  
 14. 000 TO 16. 000 82  
 16. 000 TO 18. 000 3  
 18. 000 TO 20. 000 0  
 0 GREATER THAN 20. 000 0

O TOTAL NUMBER OF ENTRIES = 9836 RMS HALF WIDTH = 5. 413

HISTOGRAM NO 10 DISTRIBUTION OF Y IN MM

HISTOGRAM NO 11 DISTRIBUTION OF X IN MM

O INTERVAL OLESS THAN -25. 000 0  
 CENTER = 2. 321 RMS HALF WIDTH = . 9836 INCLUDING UNDERFLOW AND OVERFLOW  
 -25. 000 TO -23. 000 0  
 -23. 000 TO -21. 000 0  
 -21. 000 TO -19. 000 0  
 -19. 000 TO -17. 000 0  
 -17. 000 TO -15. 000 0  
 -15. 000 TO -13. 000 0  
 -13. 000 TO -11. 000 0  
 -11. 000 TO -9. 000 0  
 -9. 000 TO -7. 000 0  
 -7. 000 TO -5. 000 0  
 -5. 000 TO -3. 000 0  
 -3. 000 TO -1. 000 0  
 -1. 000 TO 1. 000 0  
 1. 000 TO 3. 000 0  
 3. 000 TO 5. 000 0  
 5. 000 TO 7. 000 0  
 7. 000 TO 9. 000 0  
 9. 000 TO 11. 000 0  
 11. 000 TO 13. 000 0  
 13. 000 TO 15. 000 0  
 15. 000 TO 17. 000 1917  
 17. 000 TO 19. 000 2743  
 19. 000 TO 21. 000 2556  
 21. 000 TO 23. 000 1510  
 23. 000 TO 25. 000 261  
 0 GREATER THAN 25. 000 0

O TOTAL NUMBER OF ENTRIES = 9836 RMS HALF WIDTH = 1. 944 INCLUDING UNDERFLOW AND OVERFLOW

HISTOGRAM NO 11 DISTRIBUTION OF X IN MM

HISTOGRAM NO 12 DISTRIBUTION OF Y IN MM

O INTERVAL OLESS THAN -25. 000 0  
 CENTER = 18. 483 RMS HALF WIDTH = 2. 483 INCLUDING UNDERFLOW AND OVERFLOW  
 -25. 000 TO -23. 000 0  
 -23. 000 TO -21. 000 0  
 -21. 000 TO -19. 000 0  
 -19. 000 TO -17. 000 0  
 -17. 000 TO -15. 000 0  
 -15. 000 TO -13. 000 0  
 -13. 000 TO -11. 000 0  
 -11. 000 TO -9. 000 0  
 -9. 000 TO -7. 000 0  
 -7. 000 TO -5. 000 0  
 -5. 000 TO -3. 000 0  
 -3. 000 TO -1. 000 0  
 -1. 000 TO 1. 000 0  
 1. 000 TO 3. 000 0  
 3. 000 TO 5. 000 0  
 5. 000 TO 7. 000 0  
 7. 000 TO 9. 000 0  
 9. 000 TO 11. 000 0  
 11. 000 TO 13. 000 0  
 13. 000 TO 15. 000 0  
 15. 000 TO 17. 000 1917  
 17. 000 TO 19. 000 2743  
 19. 000 TO 21. 000 2556  
 21. 000 TO 23. 000 1510  
 23. 000 TO 25. 000 261  
 0 GREATER THAN 25. 000 0

O TOTAL NUMBER OF ENTRIES = 9836 RMS HALF WIDTH = 2. 483 INCLUDING UNDERFLOW AND OVERFLOW  
 HISTOGRAM NO 11 DISTRIBUTION OF X IN MM  
 HISTOGRAM NO 12 DISTRIBUTION OF Y IN MM  
 O INTERVAL OLESS THAN -25. 000 0  
 CENTER = 2183. 754 RMS HALF WIDTH = 2. 483 INCLUDING UNDERFLOW AND OVERFLOW  
 -25. 000 TO -23. 000 0  
 -23. 000 TO -21. 000 0  
 -21. 000 TO -19. 000 0  
 -19. 000 TO -17. 000 0  
 -17. 000 TO -15. 000 0  
 -15. 000 TO -13. 000 0  
 -13. 000 TO -11. 000 0  
 -11. 000 TO -9. 000 0  
 -9. 000 TO -7. 000 0  
 -7. 000 TO -5. 000 0  
 -5. 000 TO -3. 000 0  
 -3. 000 TO -1. 000 0  
 -1. 000 TO 1. 000 0  
 1. 000 TO 3. 000 0  
 3. 000 TO 5. 000 0  
 5. 000 TO 7. 000 0  
 7. 000 TO 9. 000 0  
 9. 000 TO 11. 000 0  
 11. 000 TO 13. 000 0  
 13. 000 TO 15. 000 0  
 15. 000 TO 17. 000 1917  
 17. 000 TO 19. 000 2743  
 19. 000 TO 21. 000 2556  
 21. 000 TO 23. 000 1510  
 23. 000 TO 25. 000 261  
 0 GREATER THAN 25. 000 0

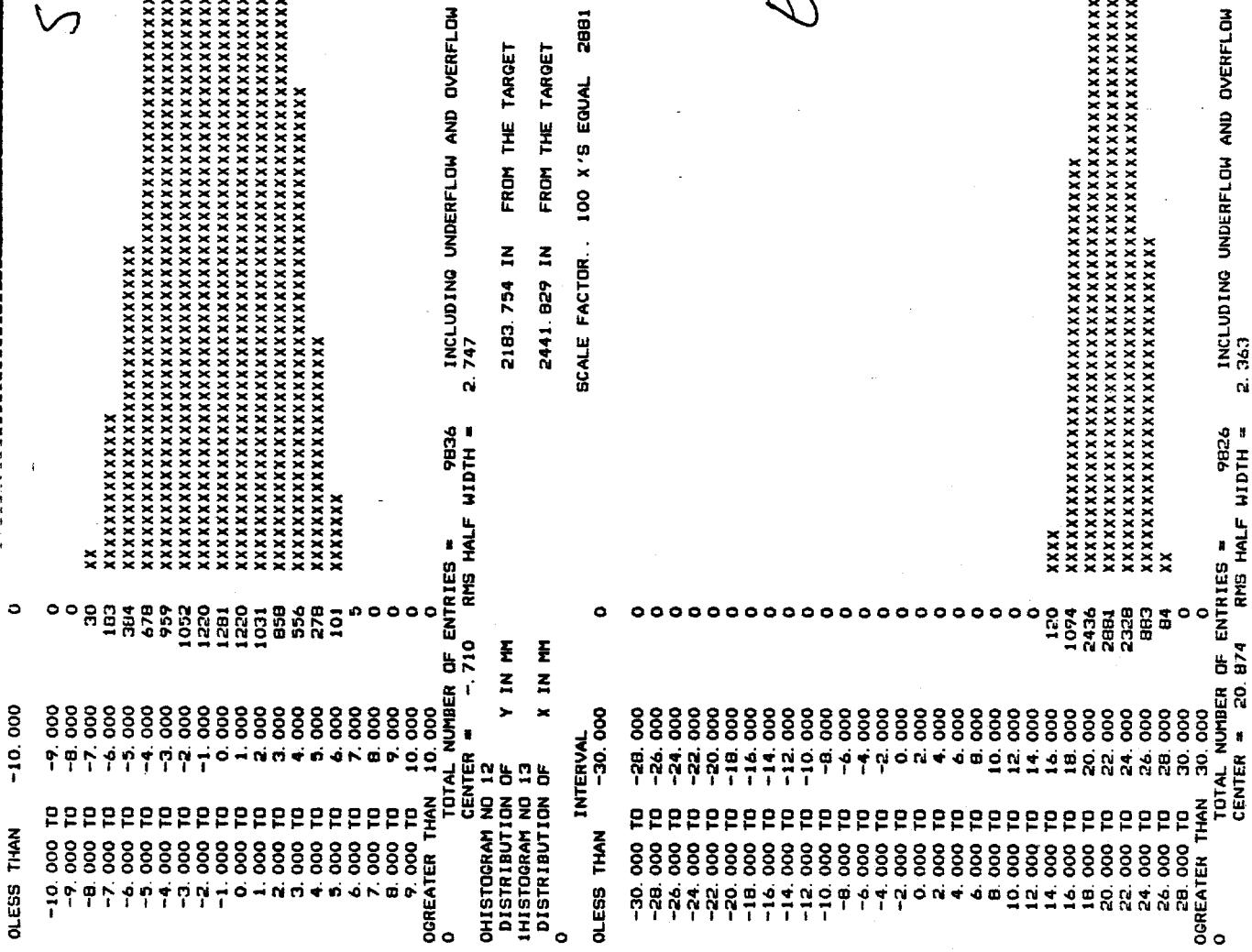
SEM 806

SEM 807

O TOTAL NUMBER OF ENTRIES = 9836 RMS HALF WIDTH = 2. 483 INCLUDING UNDERFLOW AND OVERFLOW  
 HISTOGRAM NO 11 DISTRIBUTION OF X IN MM  
 HISTOGRAM NO 12 DISTRIBUTION OF Y IN MM  
 O INTERVAL OLESS THAN -25. 000 0  
 CENTER = 2183. 754 RMS HALF WIDTH = 2. 483 INCLUDING UNDERFLOW AND OVERFLOW  
 -25. 000 TO -23. 000 0  
 -23. 000 TO -21. 000 0  
 -21. 000 TO -19. 000 0  
 -19. 000 TO -17. 000 0  
 -17. 000 TO -15. 000 0  
 -15. 000 TO -13. 000 0  
 -13. 000 TO -11. 000 0  
 -11. 000 TO -9. 000 0  
 -9. 000 TO -7. 000 0  
 -7. 000 TO -5. 000 0  
 -5. 000 TO -3. 000 0  
 -3. 000 TO -1. 000 0  
 -1. 000 TO 1. 000 0  
 1. 000 TO 3. 000 0  
 3. 000 TO 5. 000 0  
 5. 000 TO 7. 000 0  
 7. 000 TO 9. 000 0  
 9. 000 TO 11. 000 0  
 11. 000 TO 13. 000 0  
 13. 000 TO 15. 000 0  
 15. 000 TO 17. 000 1917  
 17. 000 TO 19. 000 2743  
 19. 000 TO 21. 000 2556  
 21. 000 TO 23. 000 1510  
 23. 000 TO 25. 000 261  
 0 GREATER THAN 25. 000 0

JUN 807

J-11



End of Beamline

OHISTOGRAM NO 13  
 DISTRIBUTION OF X IN MM  
 IHISTOGRAM NO 14  
 DISTRIBUTION OF Y IN MM  
 0 INTERVAL  
 OLESS THAN -10.000 0  
 -10.000 TO -9.000 0  
 -9.000 TO -8.000 0  
 -8.000 TO -7.000 0  
 -7.000 TO -6.000 5  
 -6.000 TO -5.000 971  
 -5.000 TO -4.000 2683  
 -4.000 TO -3.000 3034  
 -3.000 TO -2.000 2498  
 -2.000 TO -1.000 635  
 -1.000 TO 0.000 0  
 0.000 TO 1.000 0  
 1.000 TO 2.000 0  
 2.000 TO 3.000 0  
 3.000 TO 4.000 0  
 4.000 TO 5.000 0  
 5.000 TO 6.000 0  
 6.000 TO 7.000 0  
 7.000 TO 8.000 0  
 8.000 TO 9.000 0  
 9.000 TO 10.000 0  
 OGREATR THAN 10.000 0

TOTAL NUMBER OF ENTRIES = 9826  
 CENTER = -3.590 RMS HALF WIDTH = 1.043  
 INCLUDING UNDERFLOW AND OVERFLOW

OHISTOGRAM NO 14  
 DISTRIBUTION OF Y IN MM  
 12.13.41. UCLP, 00. TB10, 0. 814KLNS.

2441. 829 IN FROM THE TARGET  
 2441. 829 IN FROM THE TARGET  
 SCALE FACTOR.. 100 X'S EQUAL 3034 ENTRIES

J-12  
 End of Beamline

2441. 829 IN FROM THE TARGET  
 2441. 829 IN FROM THE TARGET  
 \*\* END OF LISTING \*\*

K-1

# APPENDIX K

## D/A LINE STUDIES

S. MTINGWA

11 JANUARY 1988

### PRELIMINARY SETUP

1. Setup for delayed extraction of positive secondaries from the Debuncher.
2. Reduce the number of bunches to get clean Rf capture.
3. Minimize the Debuncher injection oscillations to  $0.5 \sim 0.8$  mm in each plane.
4. Set the tunes to nominal values.
5. Do Debuncher aperture scans with heated beam.

### PREVIOUS RESULTS

1. The D/A transfer efficiency is most sensitive to the vertical beam size.
2. After blowing up the beam in the Accumulator, the transfer efficiency into the Debuncher is almost 100%.

### PROPOSED NEW STUDIES (About 1 Shift)

1. Vary cooling gate time (1 plane at a time) and monitor the Debuncher Profile Monitor, D/A Sems, D:Tor807/D:IBEAM, A:IBEAM/D:IBEAM, SEM 407 and the Gap Monitors.
2. Vary D6H6 and redo Step #1.
3. Vary the Debuncher momentum and redo the above.
4. Reset D6H6 and the Debuncher momentum; vary the current in D6Q6 by varying D:QT606 and monitor the D/A efficiency vs. the Debuncher tune.

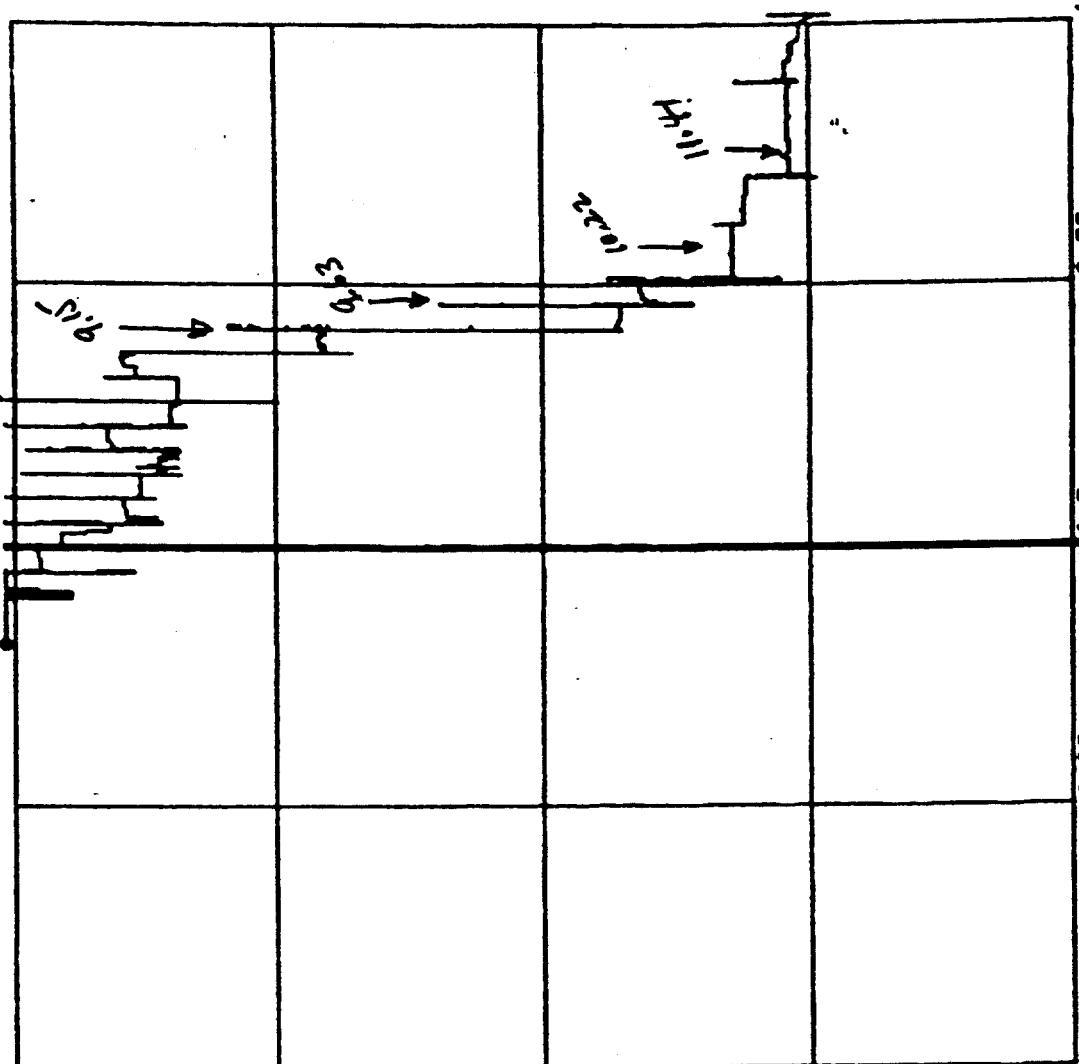
5. Vary the current in A1Q4 and monitor the D/A transfer efficiency vs. Accumulator tune.
6. From the knowledge gained above, tune the D/A transfer as best as possible and study the transfer efficiency vs. Debuncher and Accumulator bumps with particular attention on the position and angle of the beam near D6Q6 and A1Q4.

HTG. 1

singleton units

(15 Hz) X = digital A/D

13  
9.75  
6.9  
3.25  
0.6



(15 Hz)

Y=A133EAM

VOL1

0.6

1.2

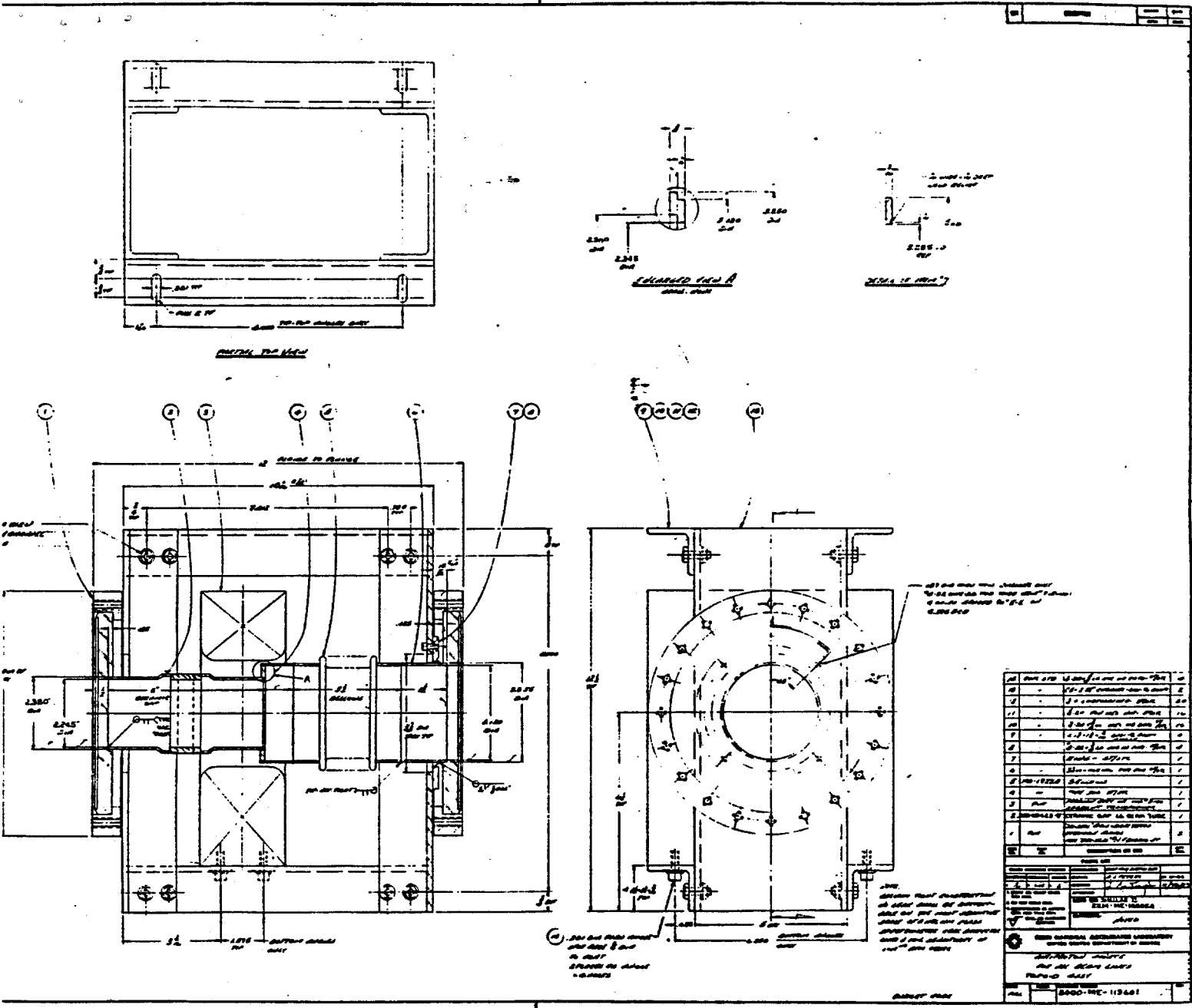
1.8

9.

SEM PRODUCTS

TALENT ART  
INDICATED SENSITIVITIES

DITD308  
OFF

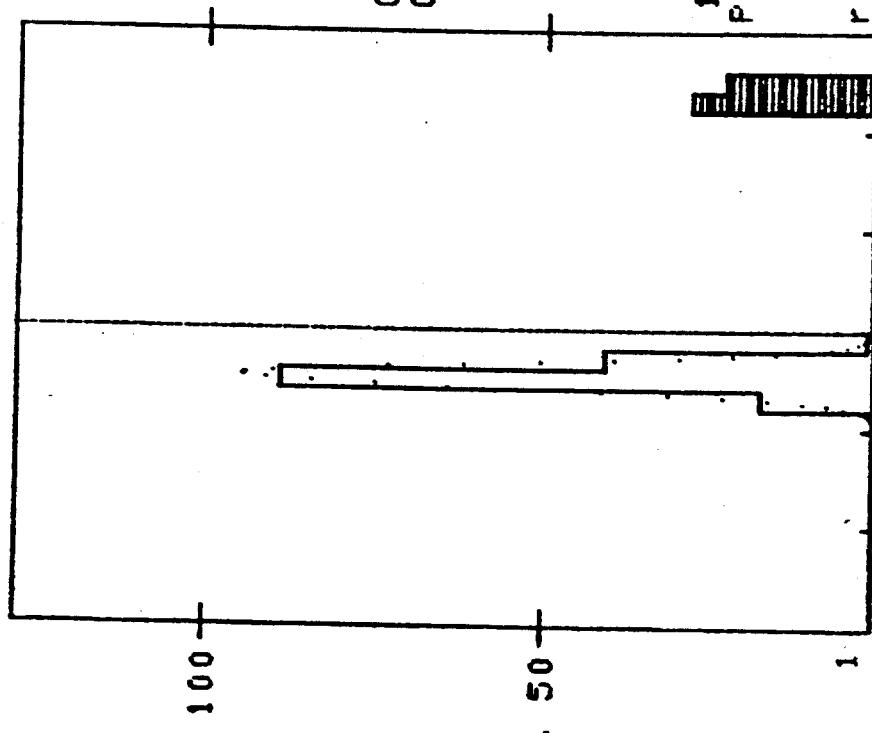


Reverse  
of rotations

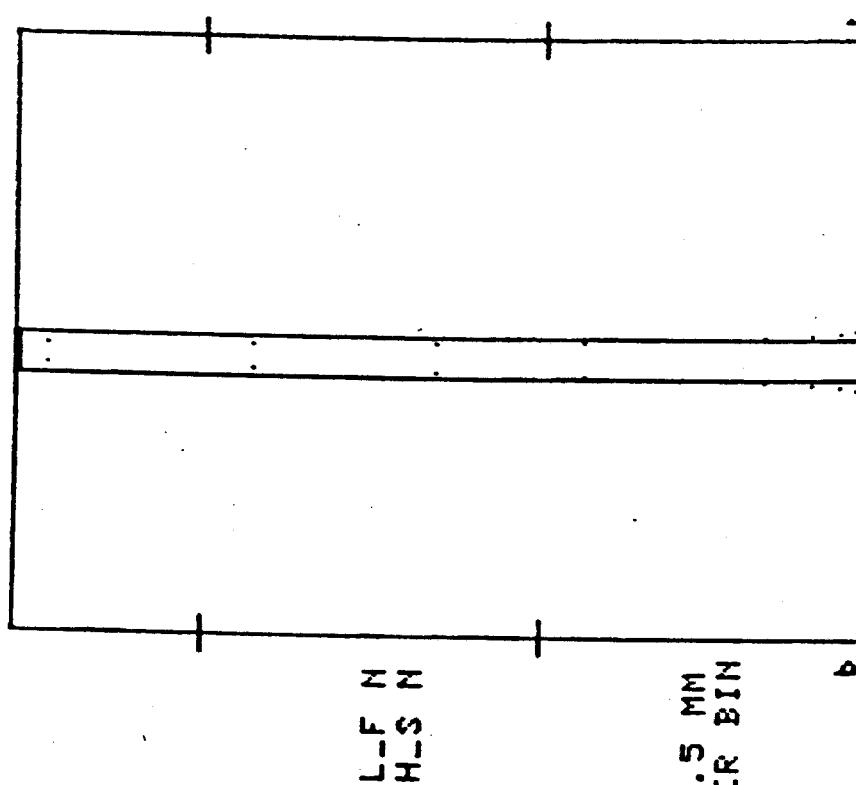
D: SH607

12/08/87 0944

X-PLOT GAIN = 1



$\gamma$ -PLOT GAIN = 1



$H_{MN} = -3.49$   $H_{SIG} = .934$   $H_{TOTAL} = 148$   $V_{MN} = -1.5$   $V_{SIG} = .75$   $V_{TOTAL} = 254$

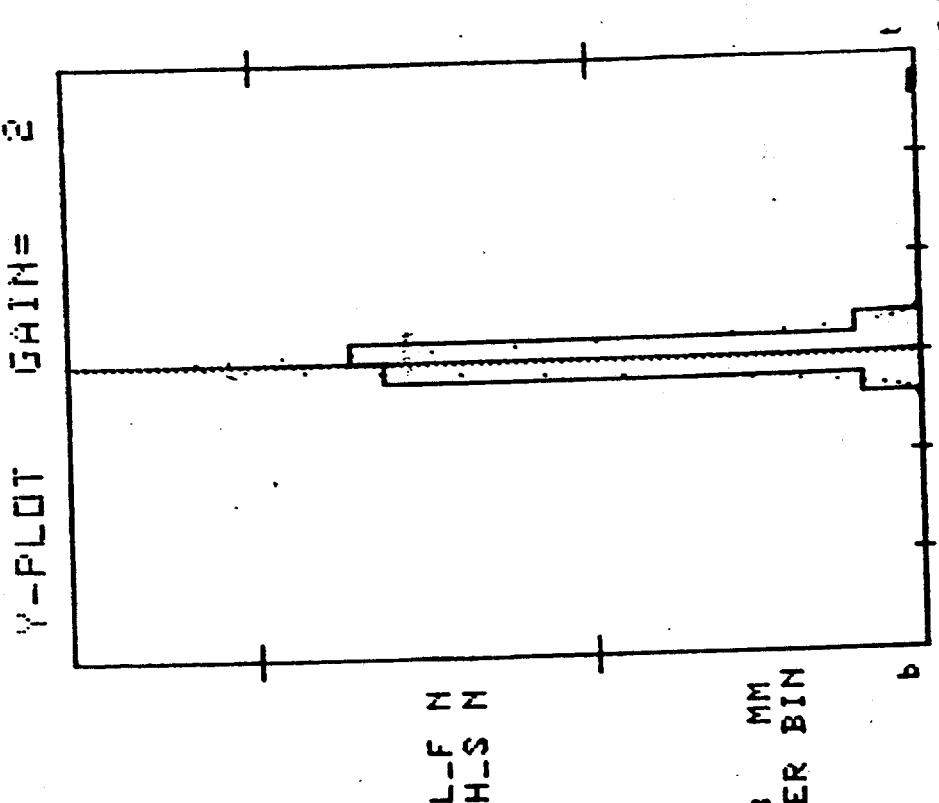
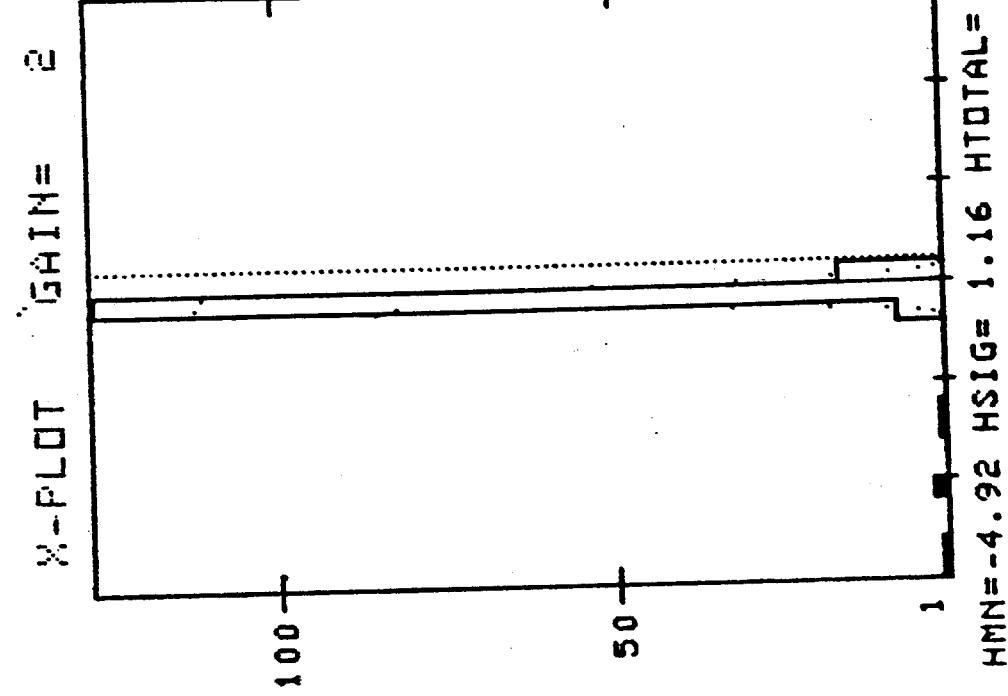
FIG. 3

Reverse Protons

NORMA 1000

D: SM802

12/08/87 0942

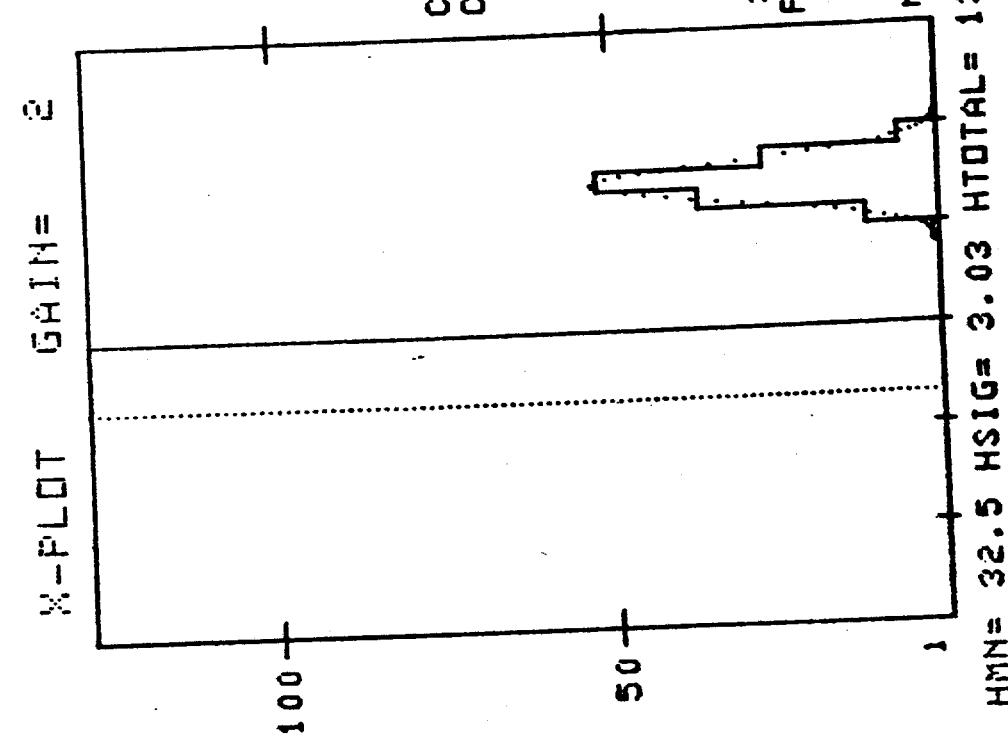


F T G. 4

## Reverse Jrotors

四三〇六

1997/08/15 09:40



HMN = 32.5 HSIG = 3.03 HUTIAL = 134

Erg. 5

REVERSE PROTONS  
Acc  $\rightarrow$  DEB.

MEASURED

D: SH807

12/08/87 0941

X- PLOT GAIN = 2

$\gamma$ - PLOT GAIN = 2

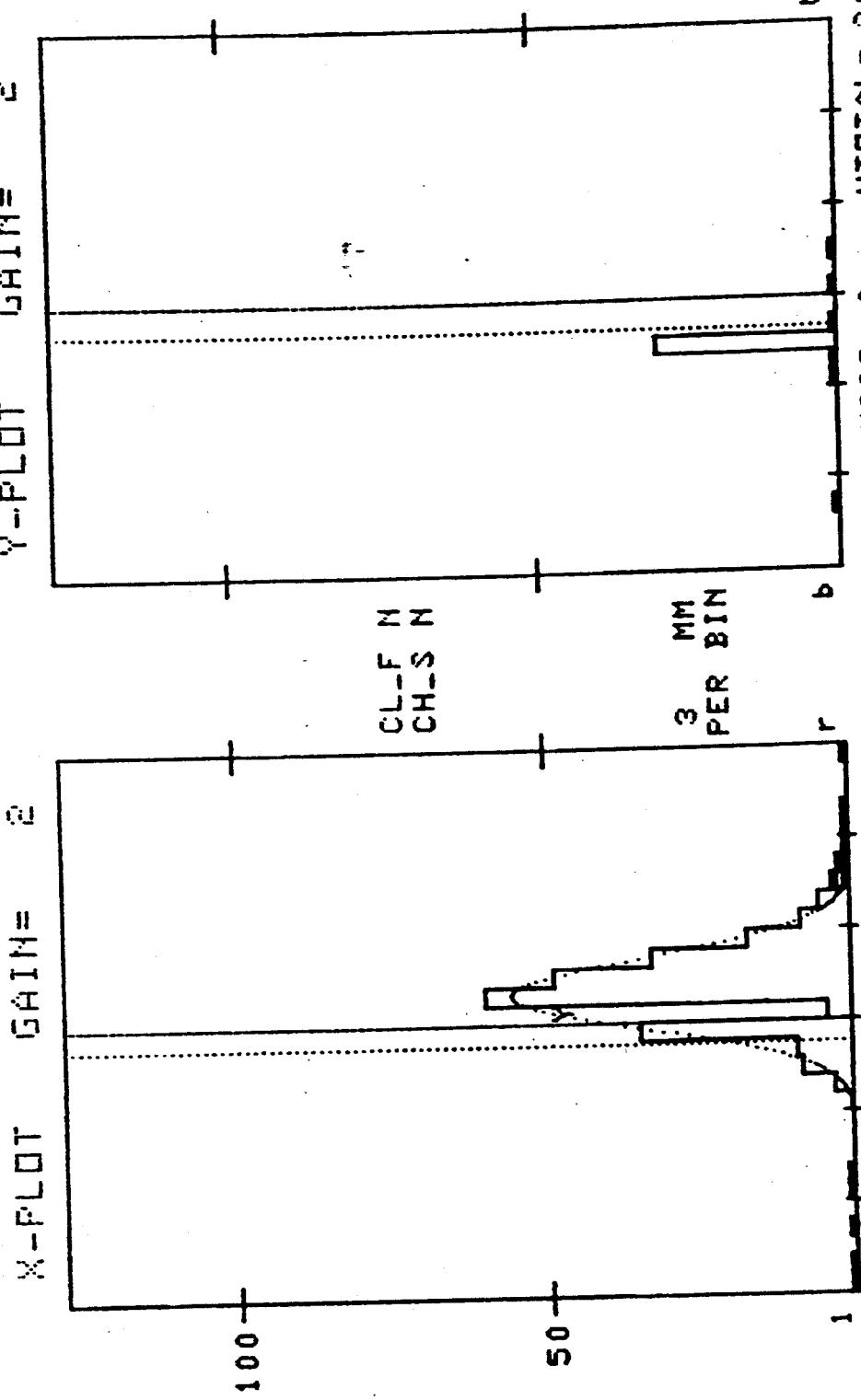


FIG. 6

Intermediate D-to-Acc. Extraction

H100M01...X

A:SM104 03/28/88 1558

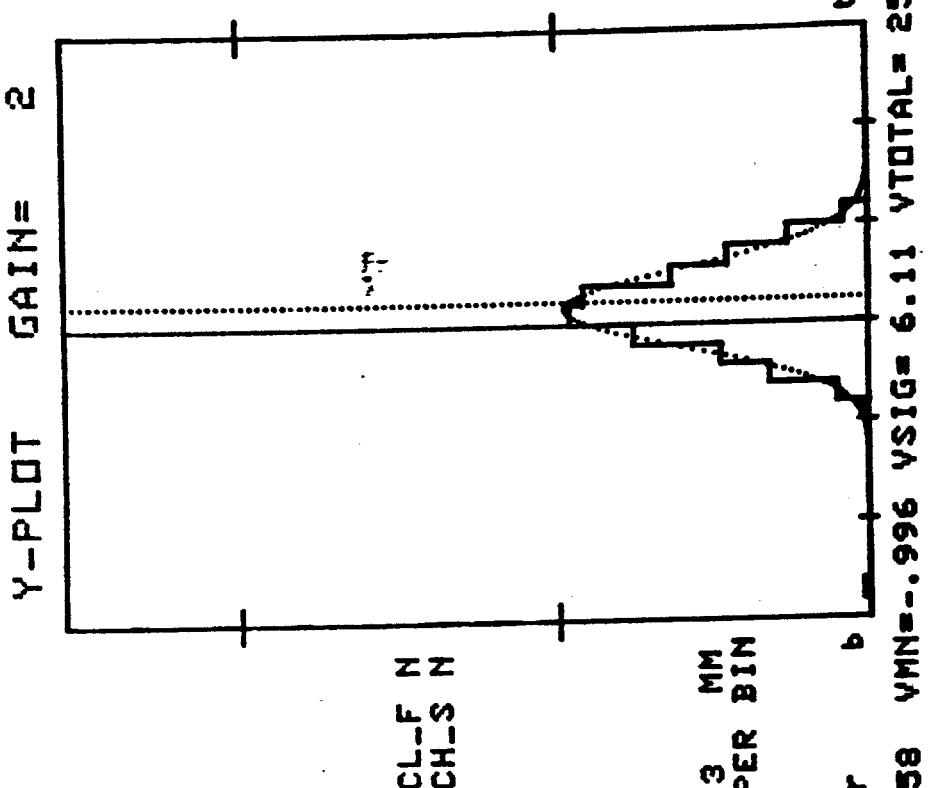
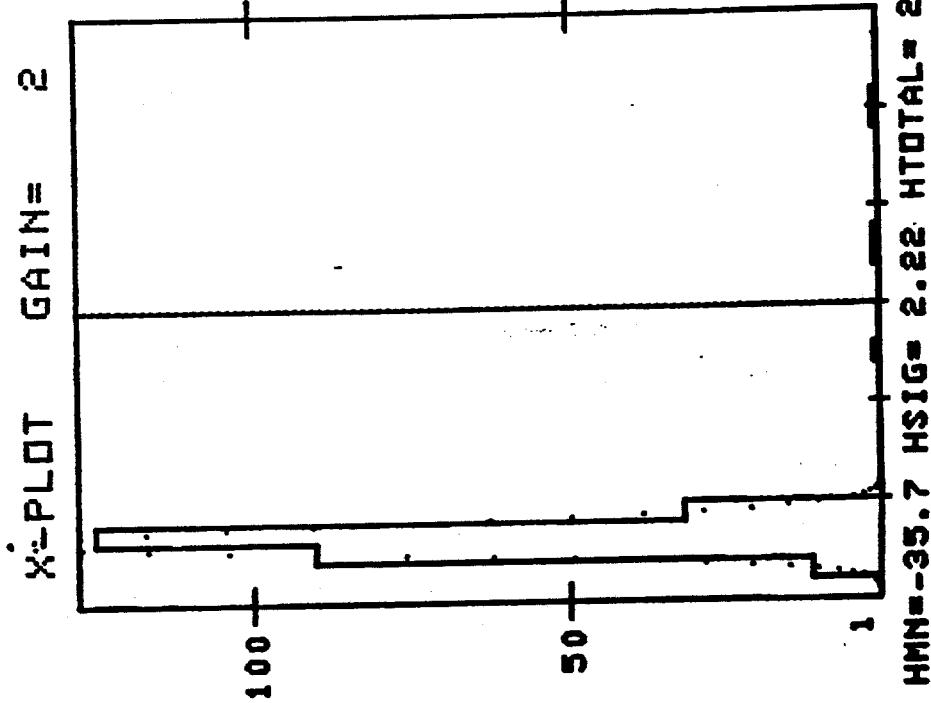


FIG. 7